



Two-phase chamber modelling of a twin-screw expander for Trilateral Flash Cycle applications

<u>Giuseppe Bianchi</u>¹, Stuart Kennedy³, Obadah Zaher², Savvas A. Tassou¹, Jeremy Miller², Hussam Jouhara¹



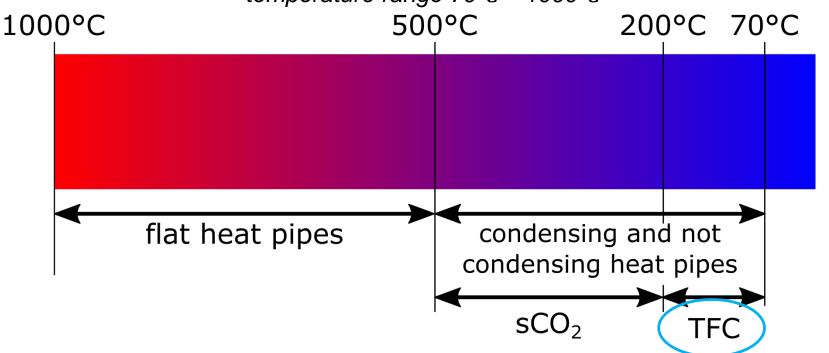






I-ThERM Project aim is to...

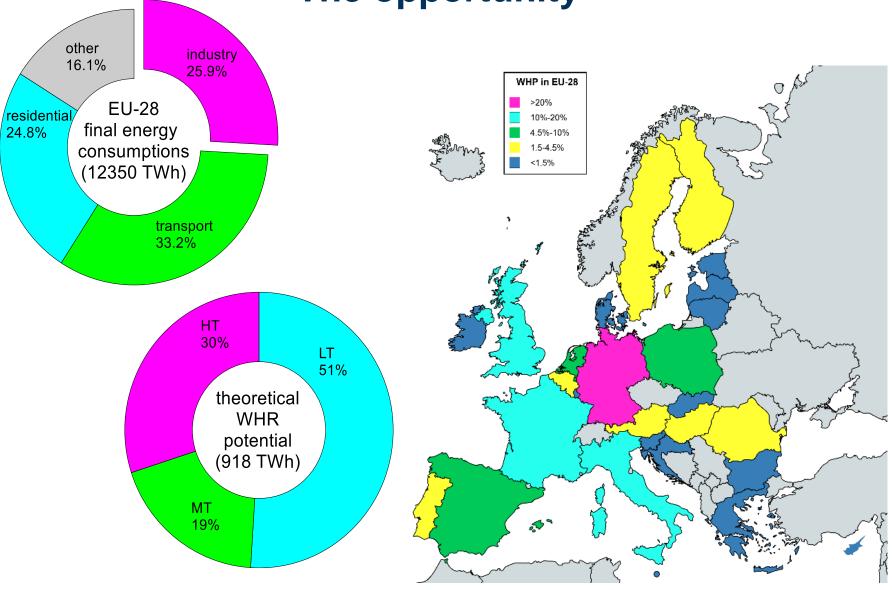
Investigate, design, build and demonstrate innovative plug and play waste heat recovery solutions to facilitate optimum utilisation of energy in selected applications with high replicability and energy recovery potential in the temperature range $70^{\circ}C - 1000^{\circ}C$





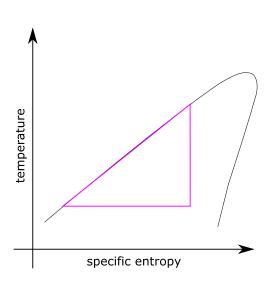
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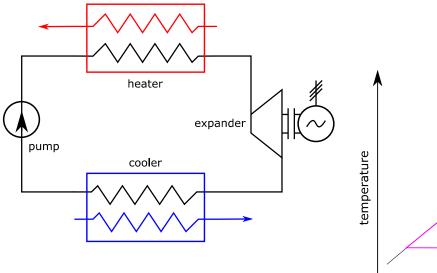
The opportunity

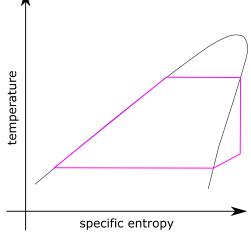


[elaborations from Eurostat database + Forman et al. 2016]

TFC vs ORC







Single phase heat recovery

- High exergetic efficiency
- High mass flow rate

Two-phase expansion

- High isentropic efficiency
- Large density changes

Multi-phase heat recovery

- Compact heater (evaporator)
- Worse heat utilization

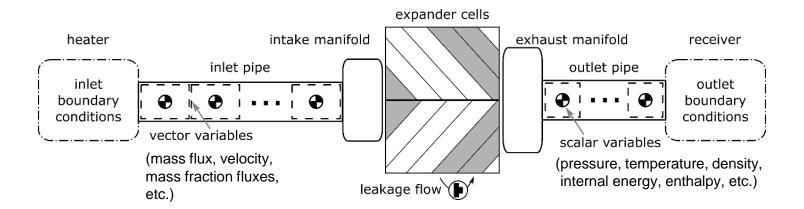
Single phase expansion

- Safer blade environment
- Realistic expansion ratios

Outline

- ✓ Potential for low grade waste heat to power conversion through TFC systems
- Modelling approach
- ☐ Input data for twin-screw machines
- ☐ Test case
- Parametric analyses
- Next challenges

Modelling approach



- One-dimensional formulation of Navier-Stokes equations
- Staggered grid spatial discretization
- Leakage paths as orifices

$$\gamma = \gamma_{vap} x + \gamma_{liq} \left(1 - x \right)$$

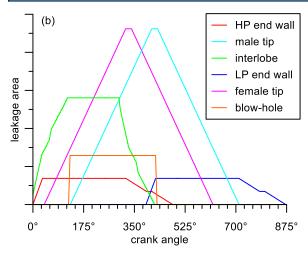
- Thermo-physical properties from REFPROP® v9.1
- Explicit Runge-Kutta scheme

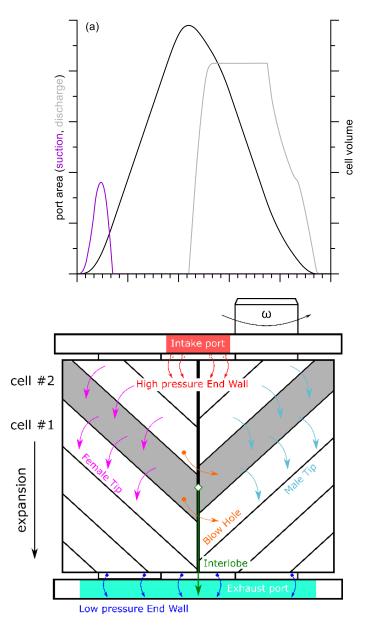


Input data

Geometrical data from pre-processor or CAD drawings

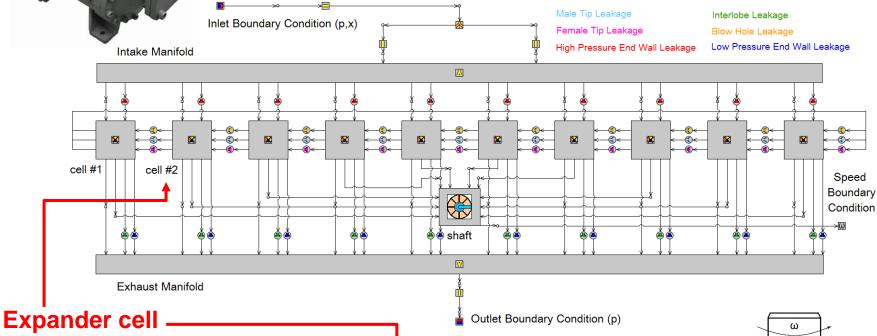
| Rotor Diameter | 127 mm |
|---------------------------------------|-----------------|
| Aspect Ratio (L/D) | 1.65 |
| Built-in Volume ratio | 5 |
| Male / Female rotor lobes | 4/6 |
| Suction / Discharge ports arrangement | axial / axial |
| Revolution speed range | 1500-6000 RPM |
| Tip speed range | 10.01-40.06 m/s |
| Weight | 220 kg |







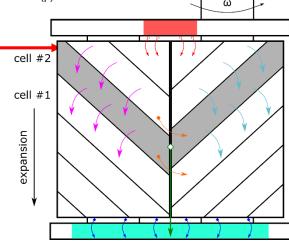
GT-SUITE® model



Scaling procedure

$$SF = 360 / \Delta \alpha = \omega_{sim} / \omega_{real}$$

$$Z_{sim} = ceil \left(\frac{\Delta \alpha \ Z_{male}}{360} \right)$$

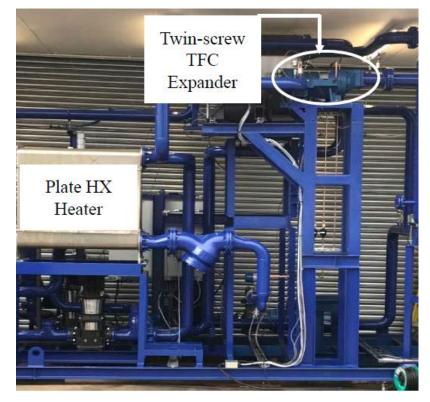


Test case – TATA Steel UK

| Stream | Flowrate (kg/s) | Inlet/max Pressure (bar) | Outlet/min Pressure (bar) | Inlet Temperature (°C) | Outlet Temperature (°C) |
|-------------------------|-----------------|--------------------------|---------------------------|------------------------|-------------------------|
| Waste heat stream | 10.39 | 4 | 3.5 | 70 | 24 |
| R245fa stream | 31.4 | 5.47 | 1.18 | 66 | 19 |
| Condensing water stream | 90.85 | 4 | 3.5 | 12 | 17 |

2MW thermal

design power output 120 kW electrical

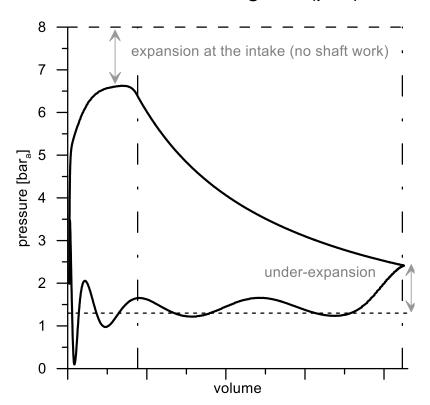


pilot test rig (1:10) at Spirax Sarco UK

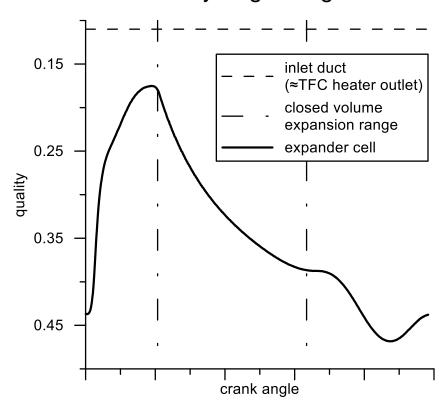
Simulation results

| Inlet pressure | Inlet quality | Revolution speed | Outlet pressure |
|--------------------|---------------|------------------|----------------------|
| 8 bar _a | 0.11 | 4070 RPM | 1.3 bar _a |

Indicator diagram (p-V)



Quality-angle diagram

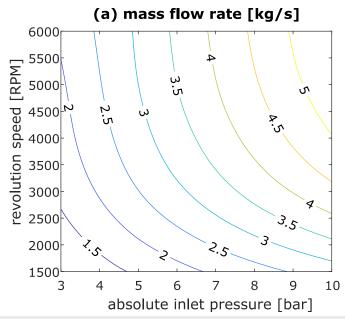


Parametric analyses

Constant inlet quality upstream the expander Variable revolution speed Inlet pressure 8bar

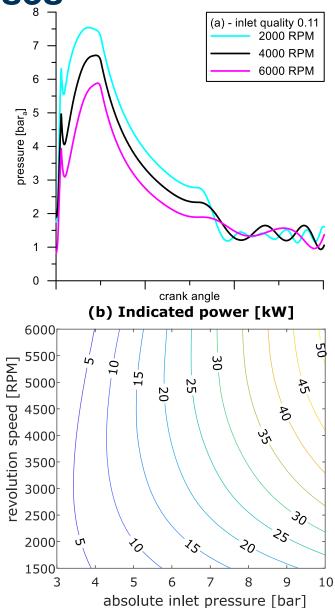
Greater revolution speeds

- Increase the expansion in the manifold
- Lower the volumetric efficiency
- Increase the indicated power, but <u>not proportionally</u>



$$\eta_{vol} = \frac{m}{\rho_{suc} V_{suc} Z_{male} \frac{\omega_{real}}{60}}$$

$$P_{ind} = Z_{male} \frac{\omega_{real}}{60} \oint p dV$$

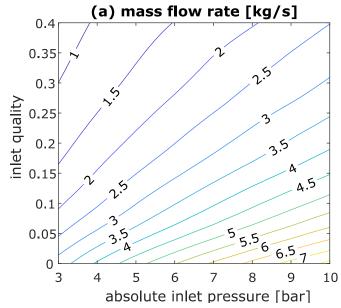


Parametric analyses (cont'd)

Constant revolution speed
Inlet quality is set upstream the expander
Inlet pressure 8bar

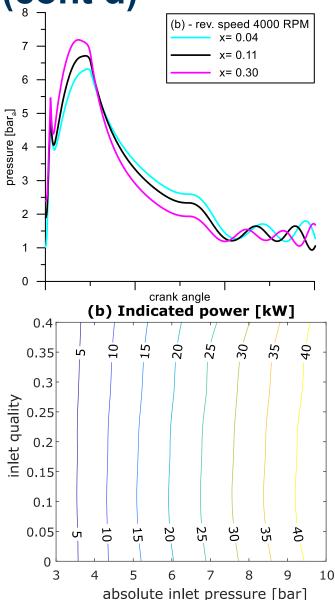
A greater inlet quality

- Lowers the mass flow rate
- Increases the volumetric efficiency
- Reduces the indicated power



$$\eta_{vol} = \frac{m}{\rho_{suc} V_{suc} Z_{male} \frac{\omega_{real}}{60}}$$

$$P_{ind} = Z_{male} \frac{\omega_{real}}{60} \oint p dV$$

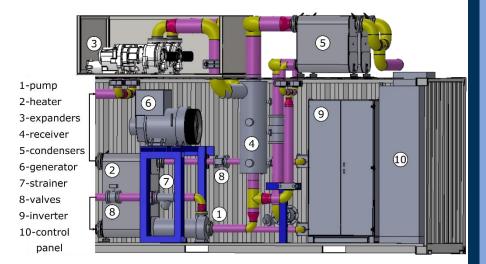


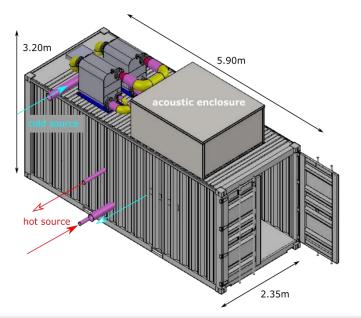
Conclusions

- Potential of low grade heat to power conversion assessed
- Similarities and differences between TFC and ORC outlined
- Modelling procedure for twin-screw machines in GT-SUITE® developed
- A twin-screw expander for TFC applications modelled
 - Pre-expansion in the intake manifold highly affects the expander performance
 - Actual expansion ratio of the Trilateral Flash Cycle is significantly influenced by the expander operation

Next challenges

- ✓ Upscaling the prototype unit
- Testing in real industrial environment
- Model setup on large size expanders
- Validation
- Transient modelling of the whole TFC system





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www.itherm-project.eu

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