

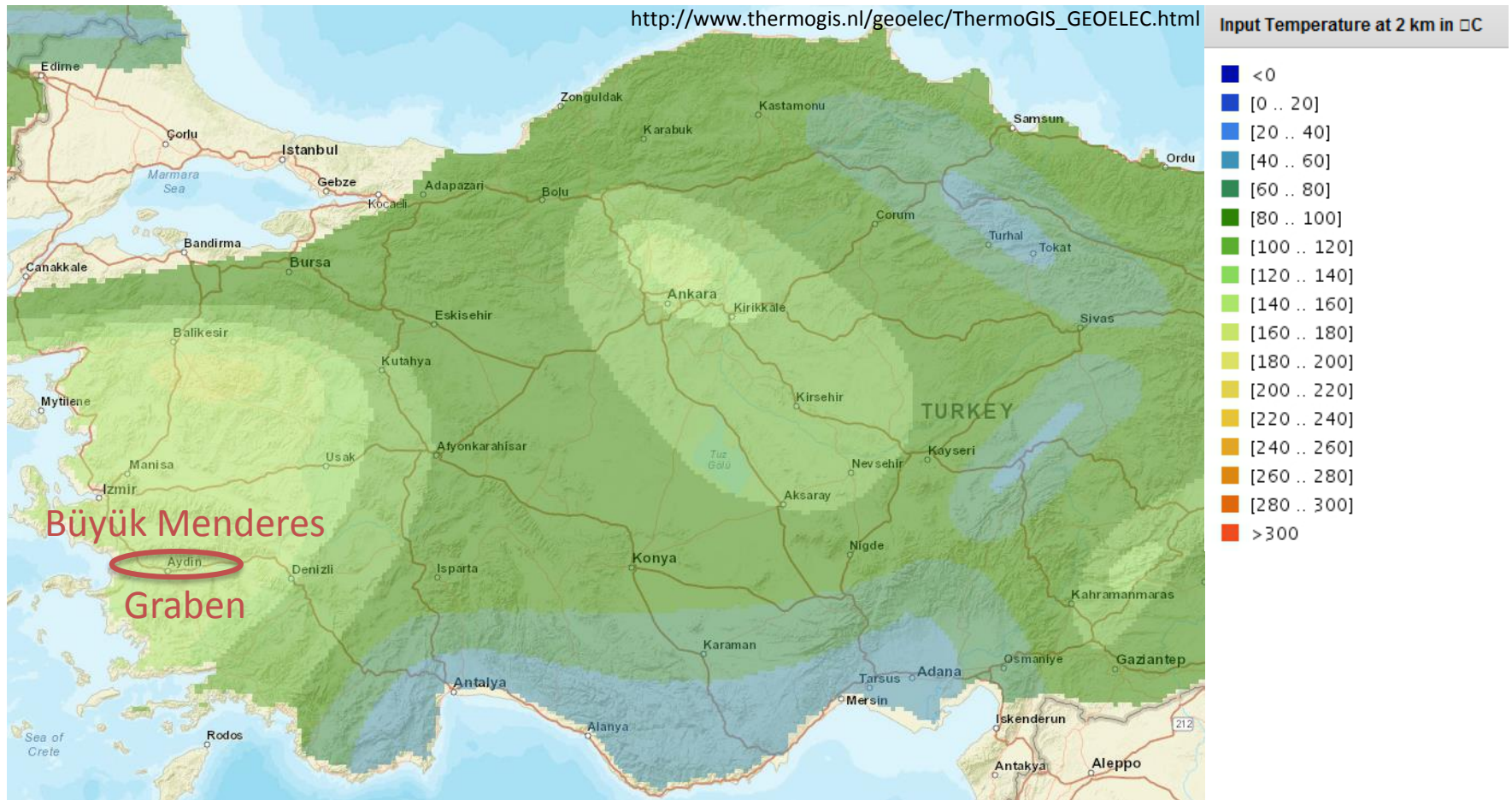
# A Retrofit for Geothermal ORC based on Concentrated Solar Thermal Systems

4th International Seminar on ORC Power Systems 2017, 13-15 Sept., Milano

F. Heberle, M. Hofer and D. Brüggemann

# Motivation

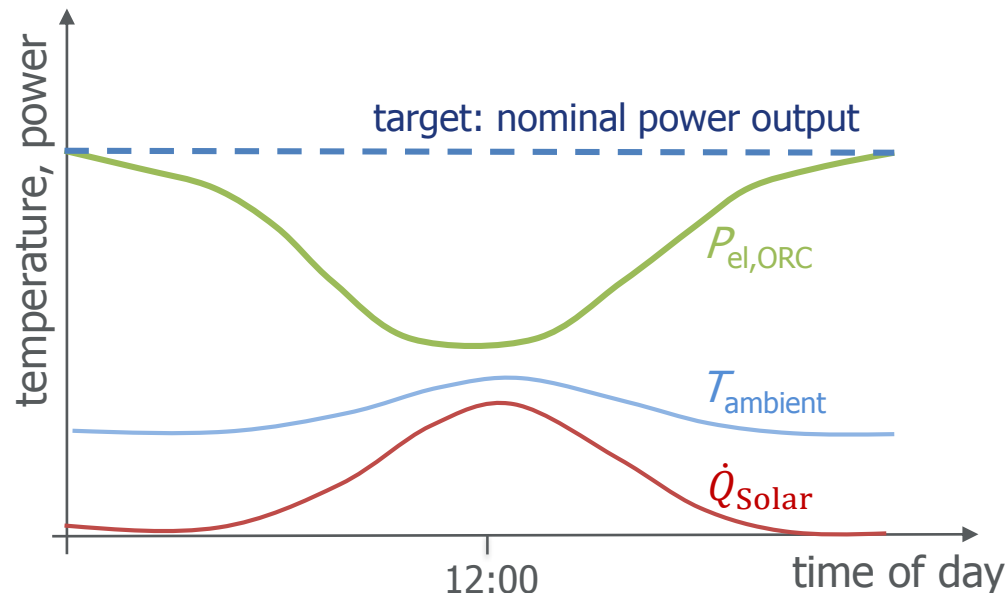
## Geothermal power generation in Turkey



# Motivation

## Geothermal power generation in Turkey – General aspects

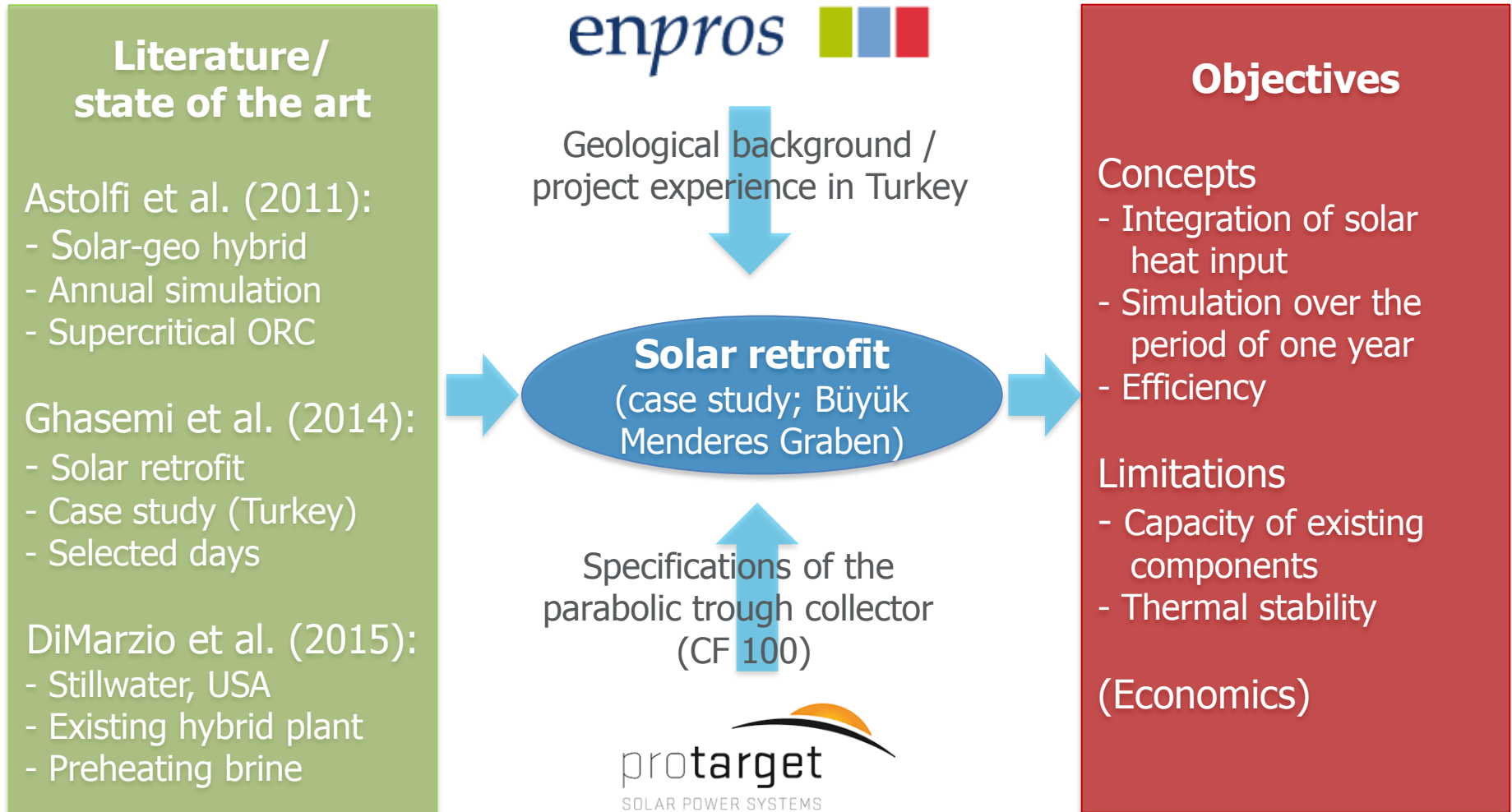
- Installed capacity\*: 650 MW<sub>el</sub> in 2015; 1284 MW<sub>el</sub> expected in 2020
- Increasing part of binary power plants (ORC) → about 320 MW<sub>el</sub> in 2016
- Air-cooled units retrofitted by (solar-thermal) parabolic trough collectors



\*M. Antics, R. Bertani, B. Sanner; *Summary of EGC 2016 Country Update Reports on Geothermal Energy in Europe*, Proceedings of the European Geothermal Congress 2016, Strassbourg (France), 2016

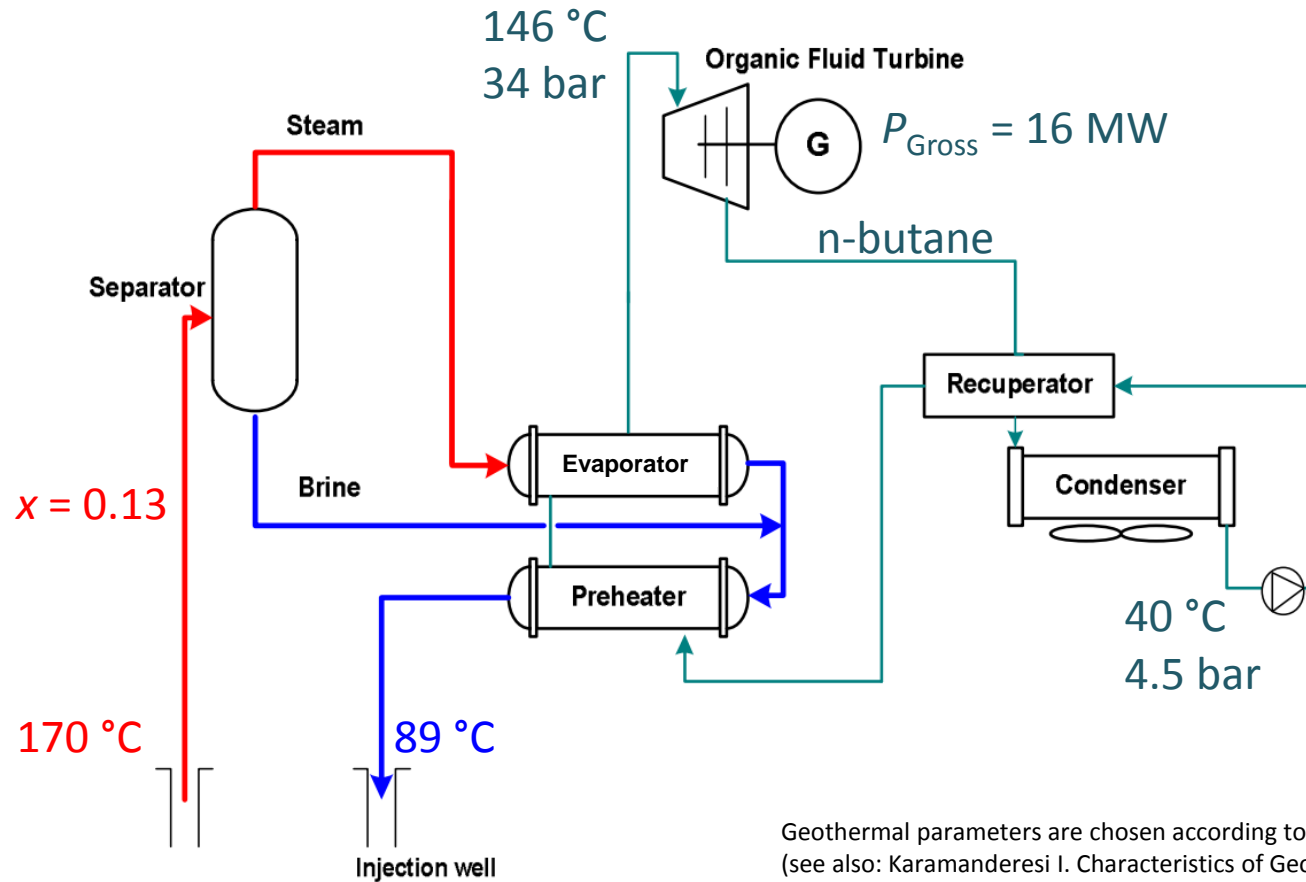
# Motivation

## Geothermal power generation in Turkey – General aspects



# Methods

## Geothermal binary power plants in Turkey – standard scheme



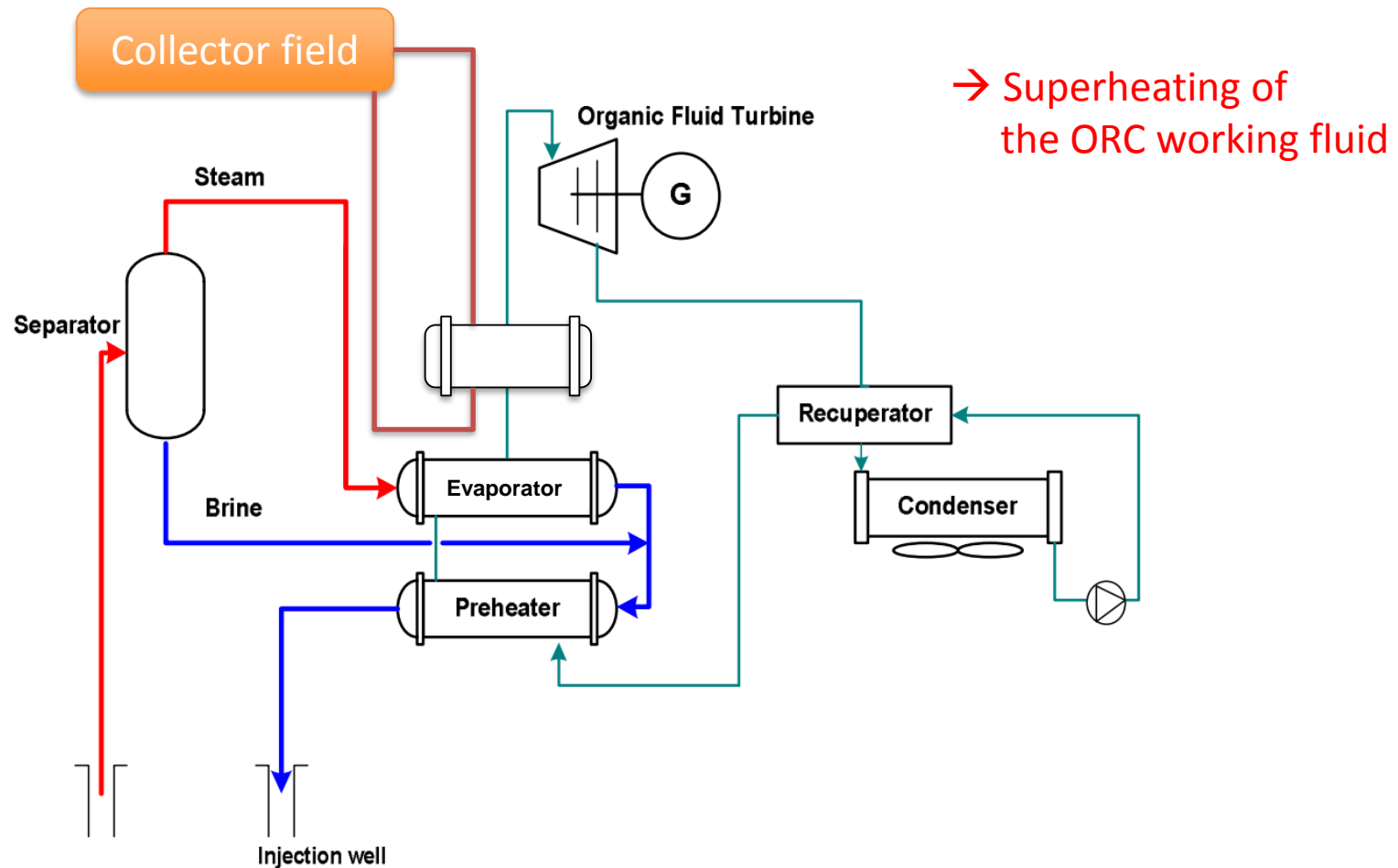
Design case

$$\vartheta_a = 18 \text{ °C}$$

Geothermal parameters are chosen according to the Aydin-Salavati field (see also: Karamanderesi I. Characteristics of Geothermal Reservoirs in Turkey. Bornova/İzmir (Turkey): 2013.)

# Methods

## Promising concept for the solar retrofit - superheater





# Methods

## Off-design calculation of the ORC unit

Turbine\*:

$$\eta_{is} = r_h r_v \eta_{is,Design} = f(\Delta h, \dot{V}_{outlet})$$

Preheater, condenser, recuperator\*\*:

$$kA_{off} = kA_{des} \left( \frac{\dot{m}_{off}}{\dot{m}_{Design}} \right)^n$$

Evaporator:

$$\Delta T_{pp} = \text{constant}$$

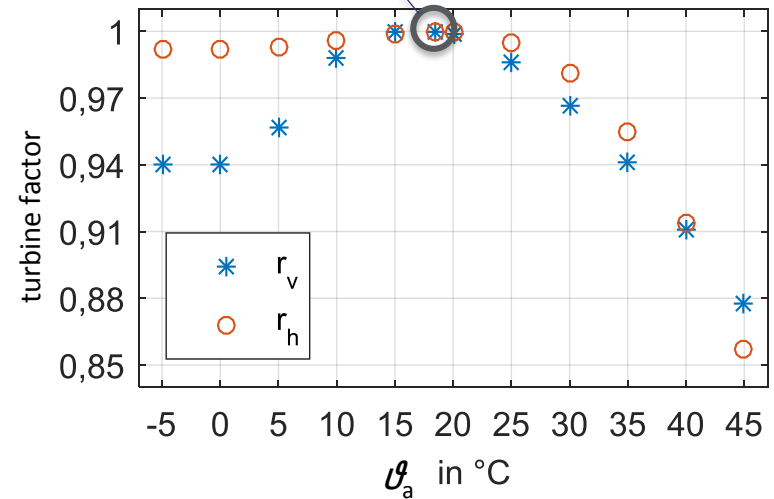
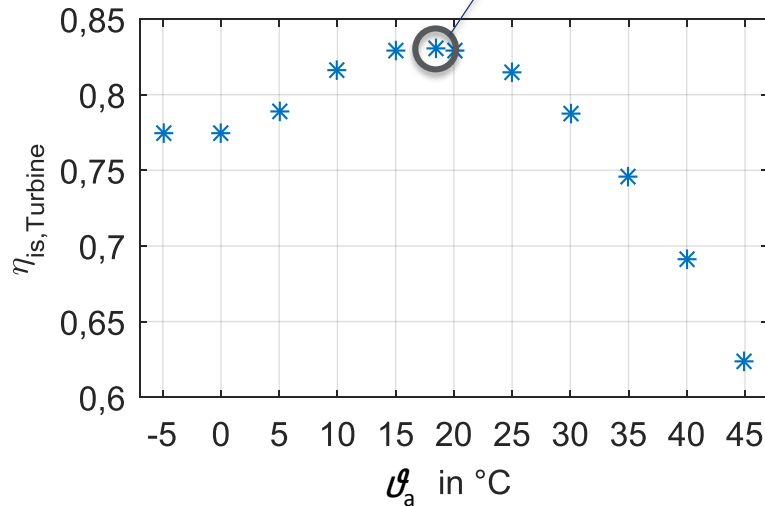
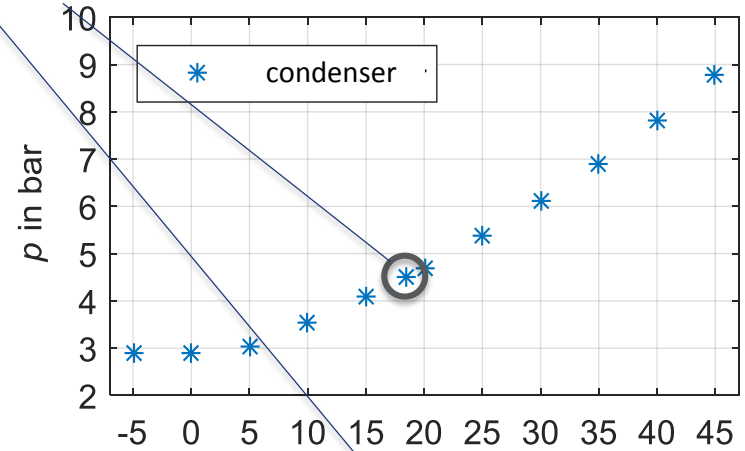
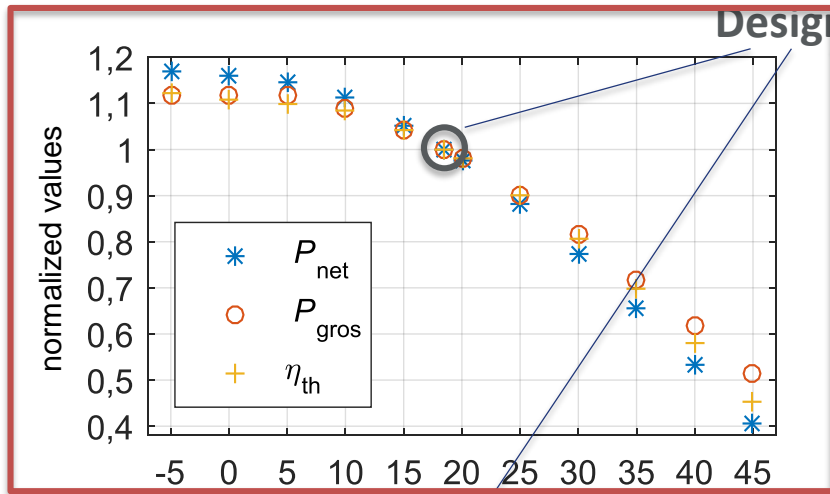
$$p_{evp} = \text{constant}; p_{cond} = f(\vartheta_a, \dot{V}_{air})$$

\*Ghasemi H, Sheu E, Tizzanini A, Paci M, Mitsos A. *Hybrid solar–geothermal power generation: Optimal retrofitting*. Appl Energy 2014;131:158–70. doi:10.1016/j.apenergy.2014.06.010.

\*\* Manente G, Toffolo A, Lazzaretto A, Paci M. *An Organic Rankine Cycle off-design model for the search of the optimal control strategy*. Energy 2013;58:97–106.

# Results

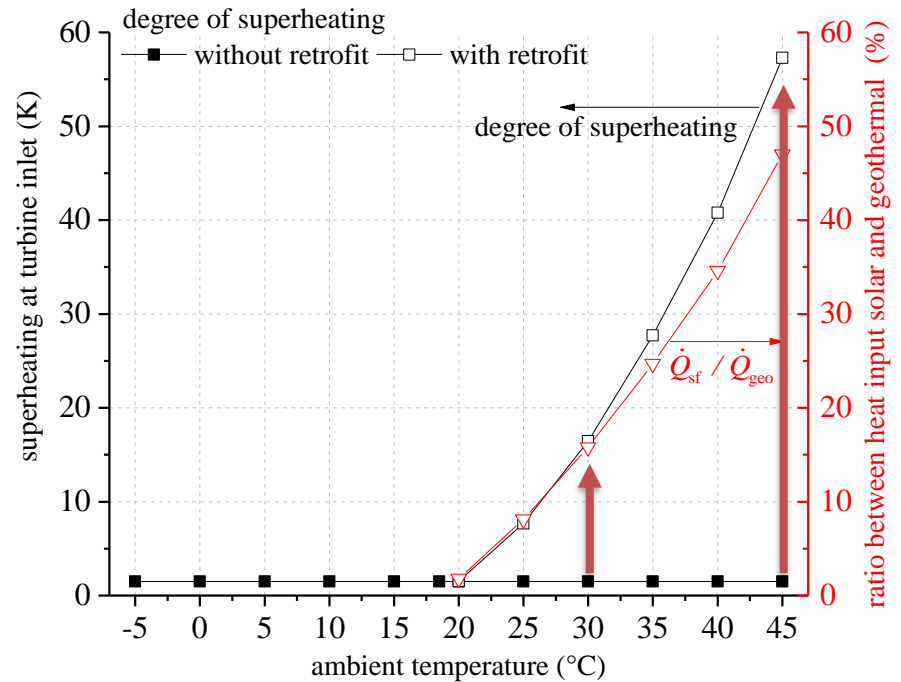
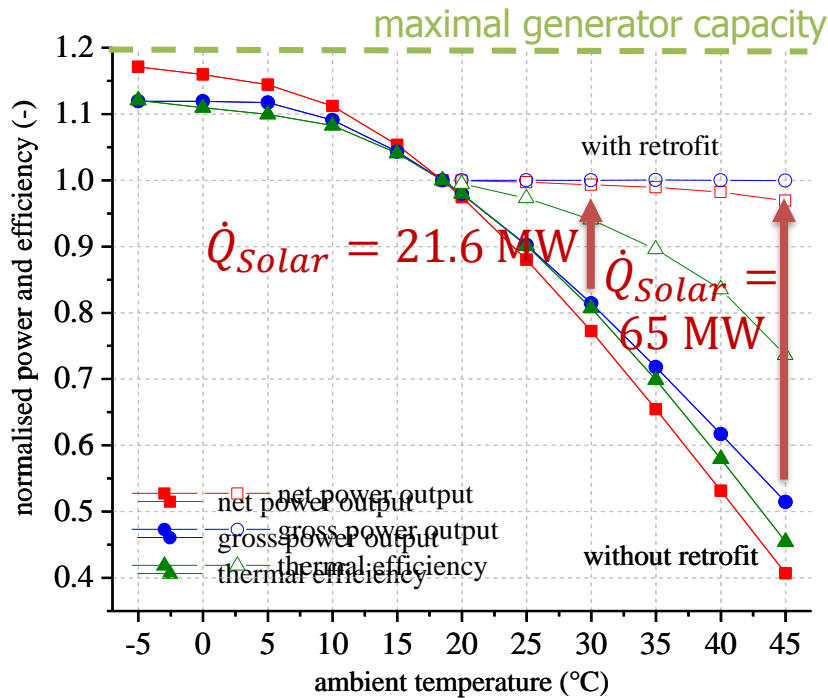
## Off-design calculation of the ORC unit





# Results

## Solar superheating – Design identification for the retrofit



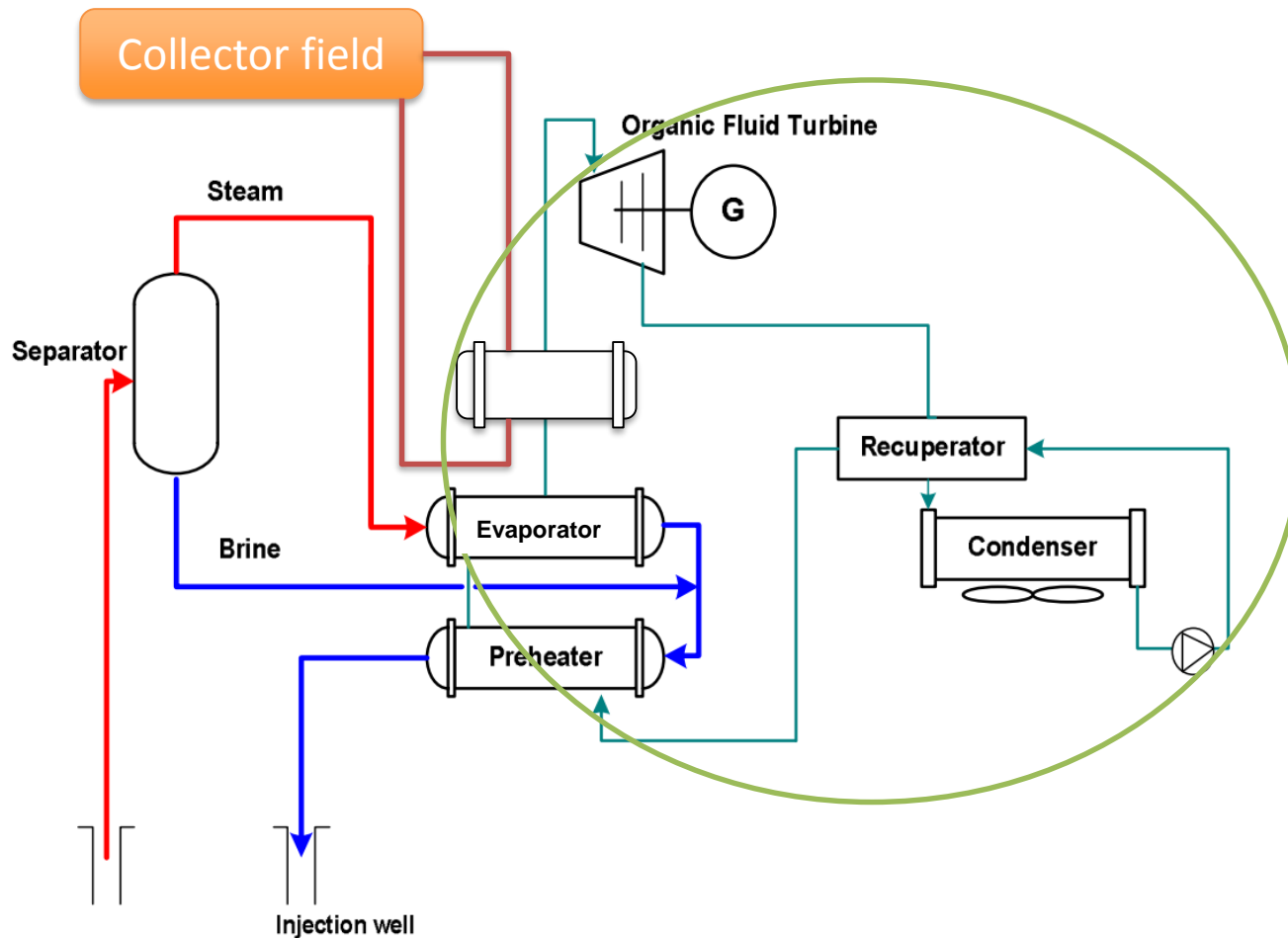
→ No problems regarding thermal stability ( $\vartheta_{\text{max,ORC}} = 200 \text{ °C}$ )\*

→ Solar heat input is limited by pump and generator capacity

\*Pasetti M, Invernizzi CM, Iora P. *Thermal stability of working fluids for organic Rankine cycles: An improved survey method and experimental results for cyclopentane, isopentane and n-butane*. Appl Therm Eng 2014;73:764–74.

# Methods II

## Solar superheating – detailed simulation over the period of one year

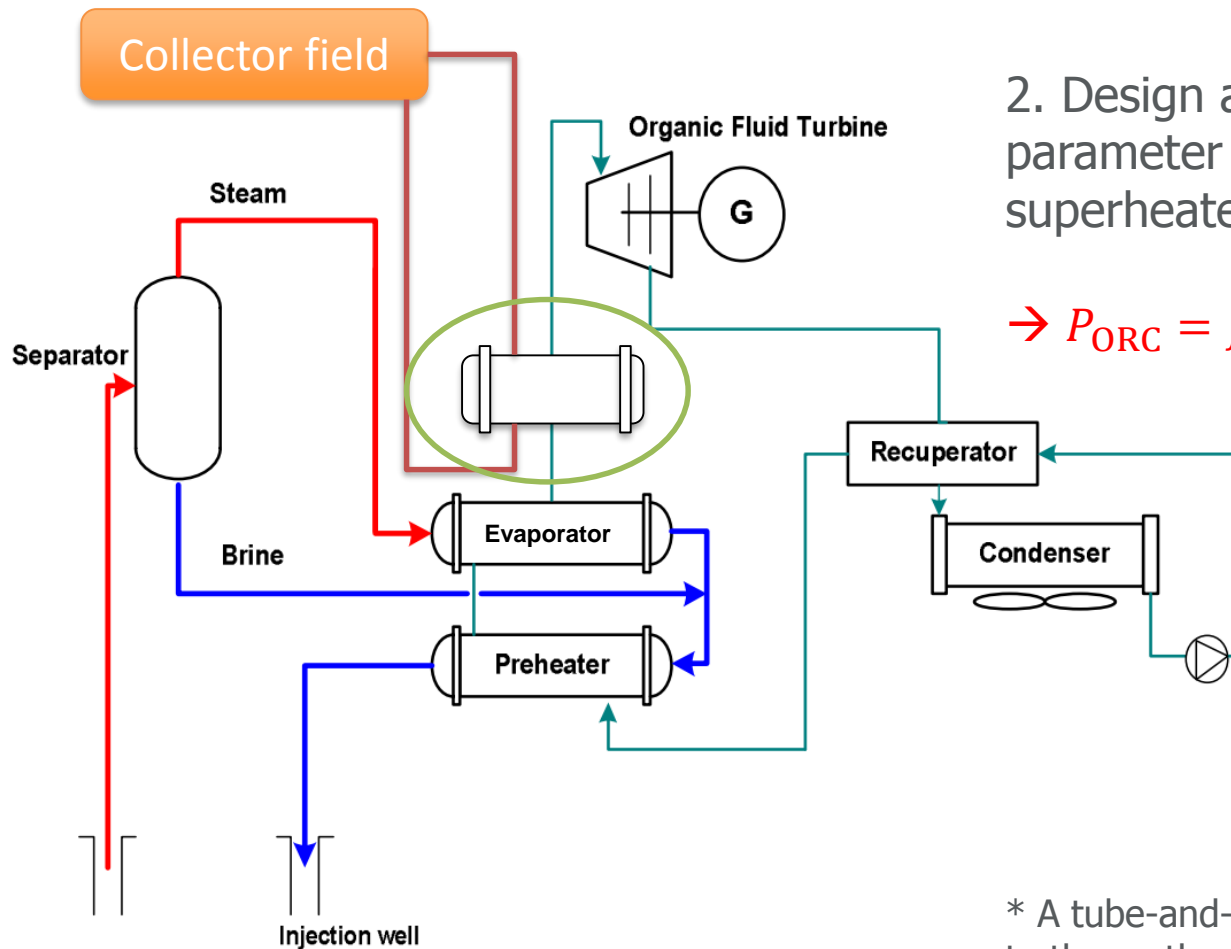


1. Operational parameter of the ORC module in Cycle-Tempo ( $\vartheta_a = -5 \dots 45 \text{ }^\circ\text{C}$ ;  $\Delta T_{SH} = 0 \dots 30 \text{ K}$ )

$$\rightarrow P_{\text{ORC}} = f(\vartheta_a, \Delta T_{\text{SH}})$$

# Methods II

## Solar superheating – detailed simulation over the period of one year



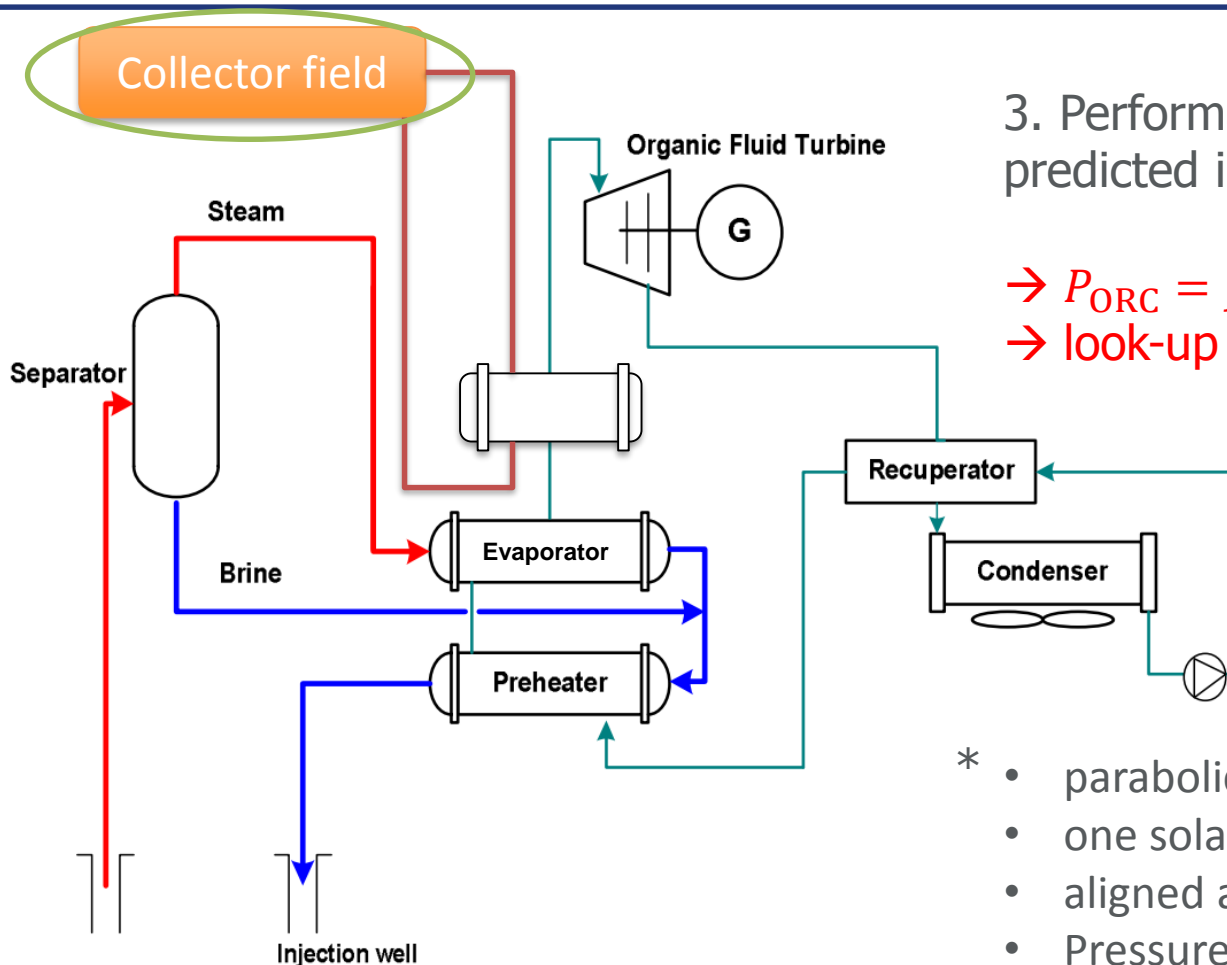
2. Design and operational parameter of the solar superheater\* in Matlab

$$\rightarrow P_{ORC} = f(\vartheta_a, \vartheta_{sf}, \dot{m}_{sf})$$

\* A tube-and-shell HEX is designed according to the method proposed by Kern. Common diameters are obtained from Kakac and Liu

## Methods II

### Solar superheating – detailed simulation over the period of one year



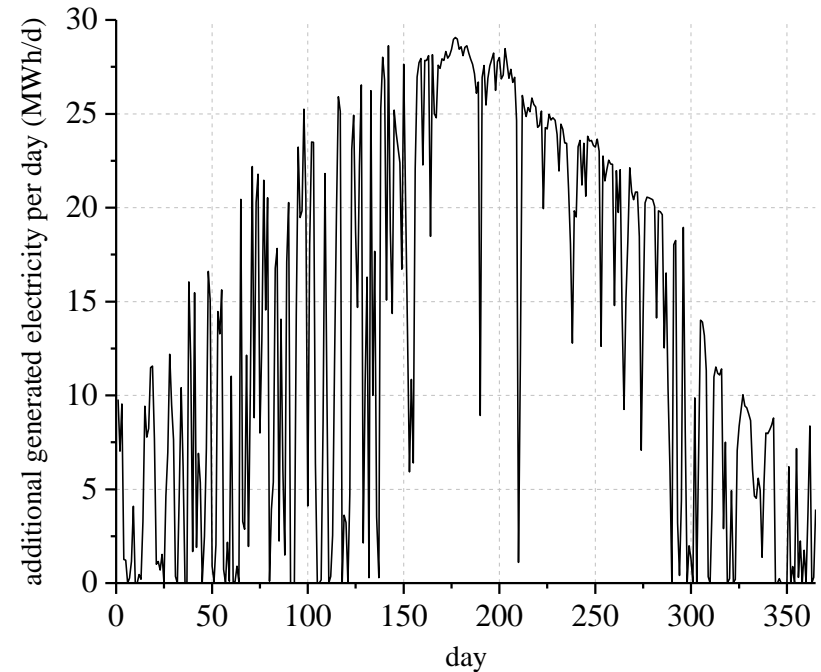
3. Performance of the solar field\* is predicted in hourly steps in Matlab

→  $P_{ORC} = f(\vartheta_a, DNI, \text{date}, \text{time})$   
→ look-up tables

- \*
  - parabolic trough collectors CF-100
  - one solar collector assembly (SCA)
  - aligned along the north-south axis
  - Pressure losses neglected
  - $\dot{Q} = \eta_{opt} \cdot \eta_{ilo} \cdot \eta_{slo} \cdot \eta_{elo} \cdot \eta_{th,sf} \cdot A_{eff} \cdot DNI$

## Results II

Simulation over period of one year – (Case 1: 21.6 MW<sub>th</sub>)



- In the summer, the retrofit provides up to 30 MWh/d additional power
- During the winter and early spring, the amount of DNI is relatively low

## Results II

### Simulation over period of one year – Variation of solar field size

| Design/performance parameter                   | unit           | value |
|--|----------------|-------|
| Solar thermal power                            | MW             | 21.6  |
| Effective area of the collectors               | m <sup>2</sup> | 32340 |
| Inlet temperature of the heat transfer fluid   | °C             | 172.3 |
| Outlet temperature of the heat transfer fluid  | °C             | 200   |
| Mass flow rate of the heat transfer fluid      | kg/s           | 178.4 |
| ORC turbine inlet temperature                  | °C             | 163.1 |
| Degree of superheating (ORC)                   | K              | 20    |
| Heat transfer area of the solar superheater    | m <sup>2</sup> | 259.5 |
| Additionally generated electricity per year    | GWh/a          | 5.2   |
| Relative increase of the generated electricity | %              | 4.5   |
| Annual solar insolation to electric efficiency | %              | 10.5  |

→ Under technical and thermodynamic criteria the retrofit is reasonable

# Conclusions

## Present study

- Superheating is not limited by thermal stability of the ORC working fluid.
- Generator and pump capacity is a constraint for the solar heat input.
- An increase of the annual generated electricity by 5 % is feasible.

## Economic aspects

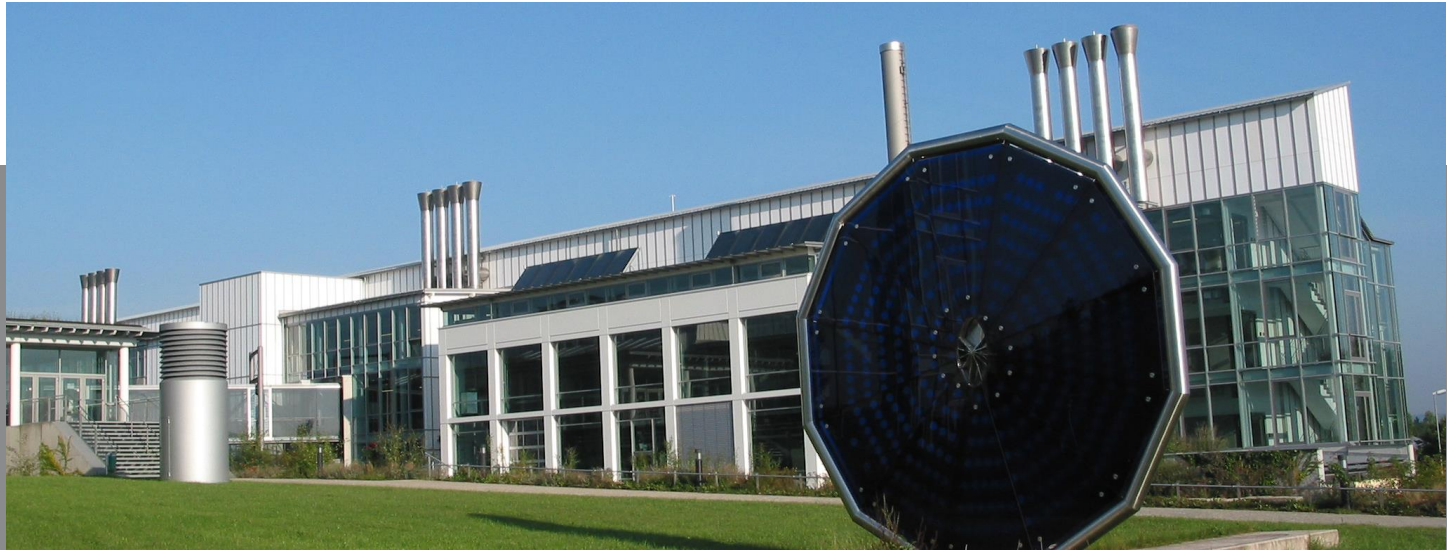
- Economic feasibility is guaranteed with a yearly DIN sum of 2086 kWh/m<sup>2</sup>.
  - 10 % increase compared to the yearly DIN average close to Sulatnhisar
  - For comparison Stillwater, Nevada (USA) yearly ID sum is 2160 kWh/m<sup>2</sup>
- For details, please see:

F. Heberle, M. Hofer, N. Ürlings, H. Schröder, T. Anderlohr, D. Brüggemann: *Techno-economic analysis of a solar thermal retrofit for an air-cooled geothermal Organic Rankine Cycle power plant*. Renewable Energy, vol. 113, pp. 494-502, doi:10.1016/j.renene.2017.06.031, June 2017



# Outlook

- Improving the model of the solar field
  - Auxiliary power requirements of the solar thermal unit and pressure losses
- Decreasing the uncertainties of the entire model
  - Reduction of the simulation step size or even a dynamic simulation
  - Available climate data
- Legal restrictions
  - Feed-in tariffs for hybrid power plants are not clearly defined
  - Land use might be regulated due to extensive agriculture



Thank you

[www.zet.uni-bayreuth.de](http://www.zet.uni-bayreuth.de)

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