



UNIVERSITY
OF FERRARA
- EX LABORE FRUCTUS -

DE Department of
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Experimental and numerical characterization of an oil-free scroll expander

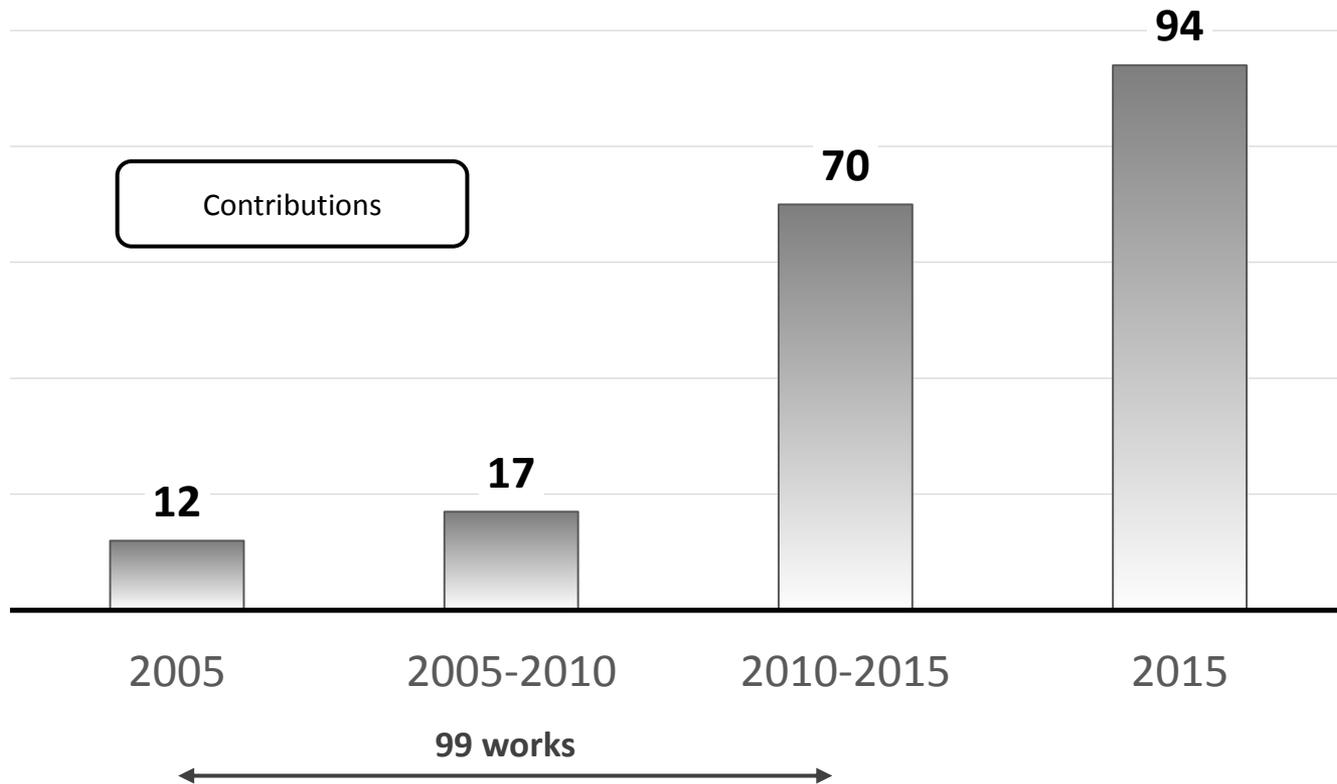
Milan, September 15, 2017

4th International seminar on
ORC Power Systems



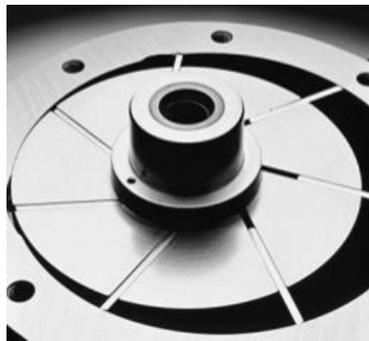
Introduction – 1

Organic
Rankine
Cycle



Organic
Rankine
Cycle

Expander



Scroll Hermetic

Gerotor

Scroll

Pneumatic Drill

Rotary Vane

Turbine Radial

Turbine Axial

Swash-plate Piston

Screw Single

Screw Twin

Scroll Open-Drive

Rolling-piston

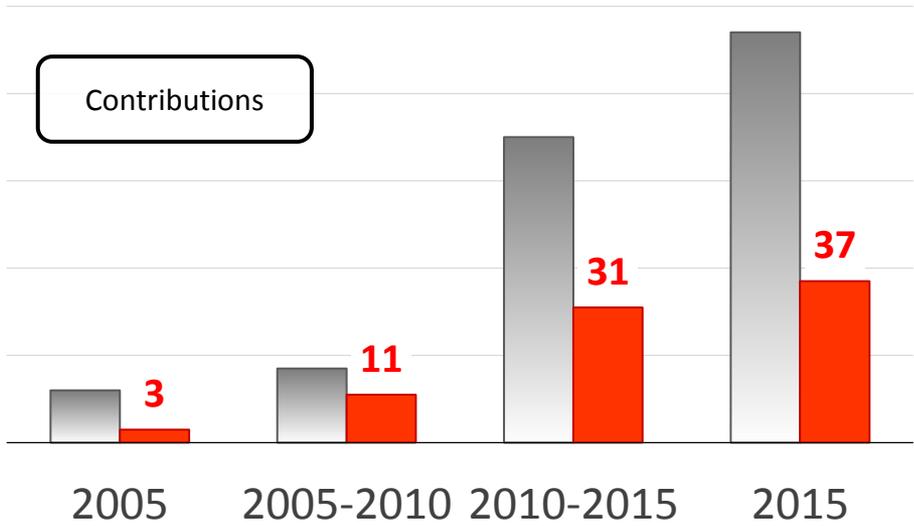
Scroll Semi-Hermetic

Piston

Introduction – 3

Organic Rankine Cycle

Expander



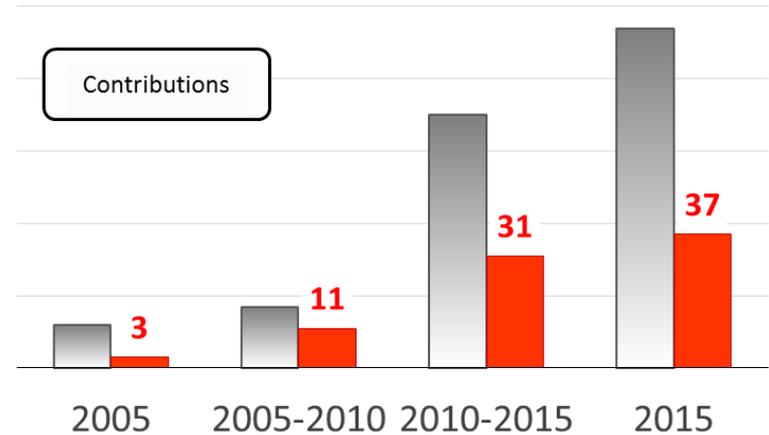
82 on 193 refer to Scroll

- Scroll Hermetic
- Gerotor
- Scroll
- Pneumatic Drill
- Rotary Vane
- Turbine Radial
- Turbine Axial
- Swash-plate Piston
- Screw Single
- Screw Twin
- Scroll Open-Drive
- Rolling-piston
- Scroll Semi-Hermetic
- Piston



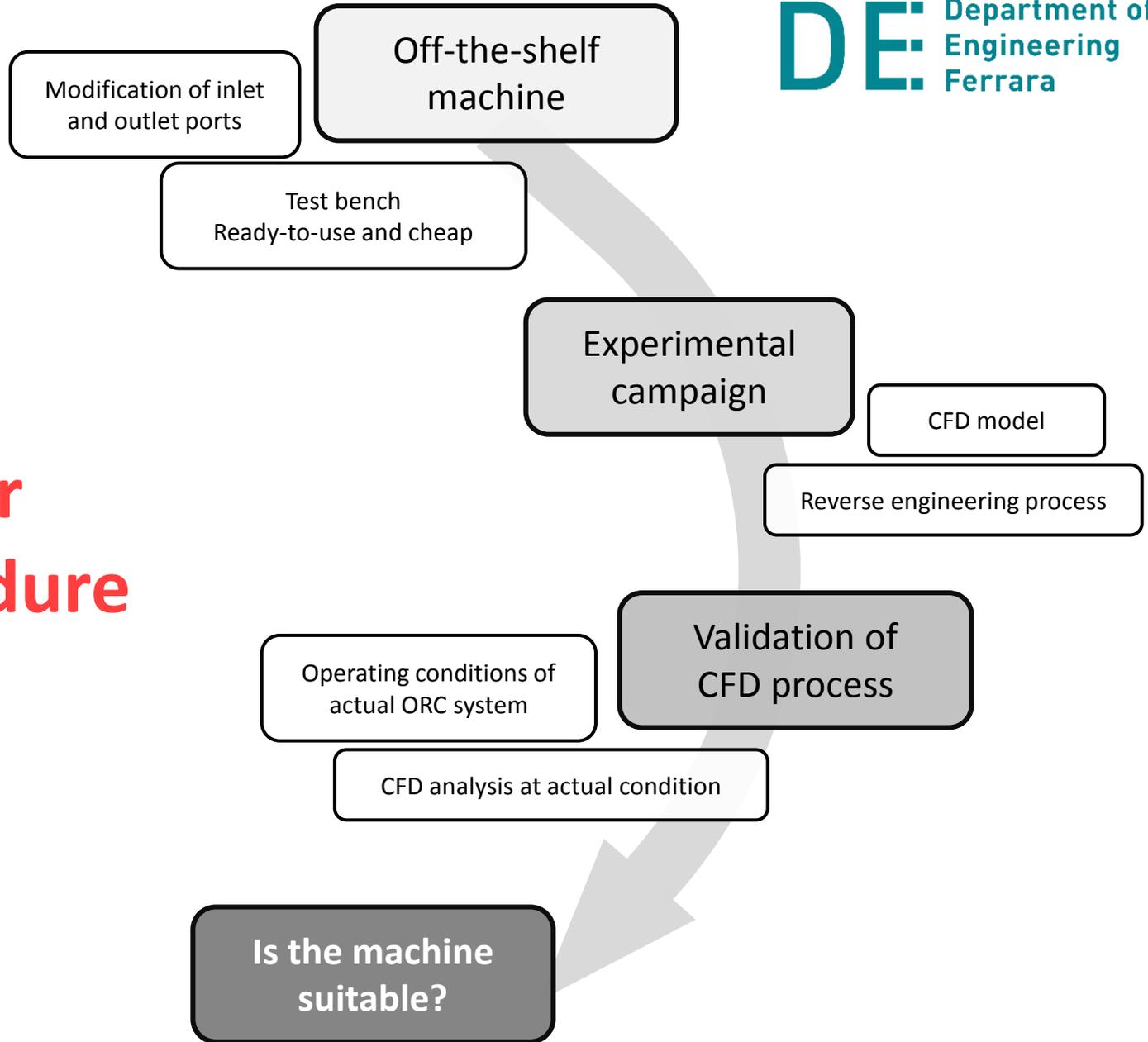
Introduction – 4

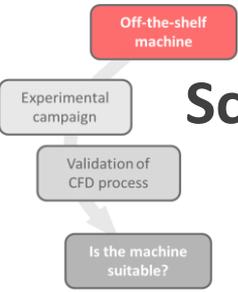
Scroll Expander
Usually $P_{el} < 2$ kW



Researchers	Expander type	Working fluids	Isentropic efficiency (%)	Power [kW]	Rotate speed [rpm]	Pressure ratio
Yamamoto et al. [150]	Radial-inflow turbine	R123	48	0.15	17,000	-
Nguyen et al. [151]	Radial-inflow turbine	<i>n</i> -pentane	49.8	1.44	65,000	3.45
Yagoub et al. [152]	Radial-inflow turbine	HFE-301	85	1.50	60,000	1.1
	<i>n</i> -pentane		40	1.50	60,000	1.3
Inoue et al. [153]	Radial-inflow turbine	TFE	70–85	5–10	15,000–30,000	4.8
Kang [154]	Radial-inflow turbine	R245fa	78.7	32.7	63,000	4.11
Pei et al. [155]	Radial-inflow turbine	R123	65	1.36	24,000	5.2
Li et al. [156]	Radial-inflow turbine	R123	68	2.40	40,000	6.3
Zanelli and Favrat [157]	Scroll expander	R134a	63–65	1–3.5	2400–3600	2.4–4.0
Mathias et al. [158]	Scroll expander	R123	67, 81, 83	1.2, 1.38, 1.75	3670	8.8, 5.5, 3.1
Peterson et al. [159]	Scroll expander	R123	45–50	0.14–0.24	600–1400	3.28–3.87
Wang et al. [88]	Scroll expander	R134a	70–77	0.5–0.8	1015–3670	2.65–4.84
Saitoh et al. [160]	Scroll expander	R113	65	0–0.46	1800–4800	-
Kim et al. [161]	Scroll expander	Water	33.8	11–12	1000–1400	10.54–11.5
Manolakos et al. [162]	Scroll expander	R134a	10–65	0.35–2	300–390	-
Lemort et al. [86,87]	Scroll expander	R123	42.5–67	0.4–1.8	1771–2660	2.75–5.4
	Scroll expander	R245fa	45–71	0.2–2	-	2–5.7
Guangbin et al. [163]	Scroll expander	Air	-	0.4–1.1	1740–2340	3.66
Wang et al. [164]	Screw expander	Air	26–40	0.5–3	400–2900	-
Smith et al. [165]	Screw expander	R113	48–76	6–15.5	1300–3600	2.11
Baek et al. [166]	Reciprocating piston expander	CO ₂	10.5	24.35	114	2.1
Zhang et al. [167]	Reciprocating piston expander	CO ₂	62	-	306	2.4
Mohd et al. [101]	Rotary vane expander	R245fa	43–48	0.025–0.032	2200–3000	21.54–24.1
Yang et al. [102]	Rotary vane expander	CO ₂	17.8–23	-	300–1500	7
Qiu et al. [168]	Rotary vane expander	HFE7000	52.88–55.45	1.66–1.7	841–860	2.063–2.09

Our Procedure





Scroll Compressor



Stator



Rotor

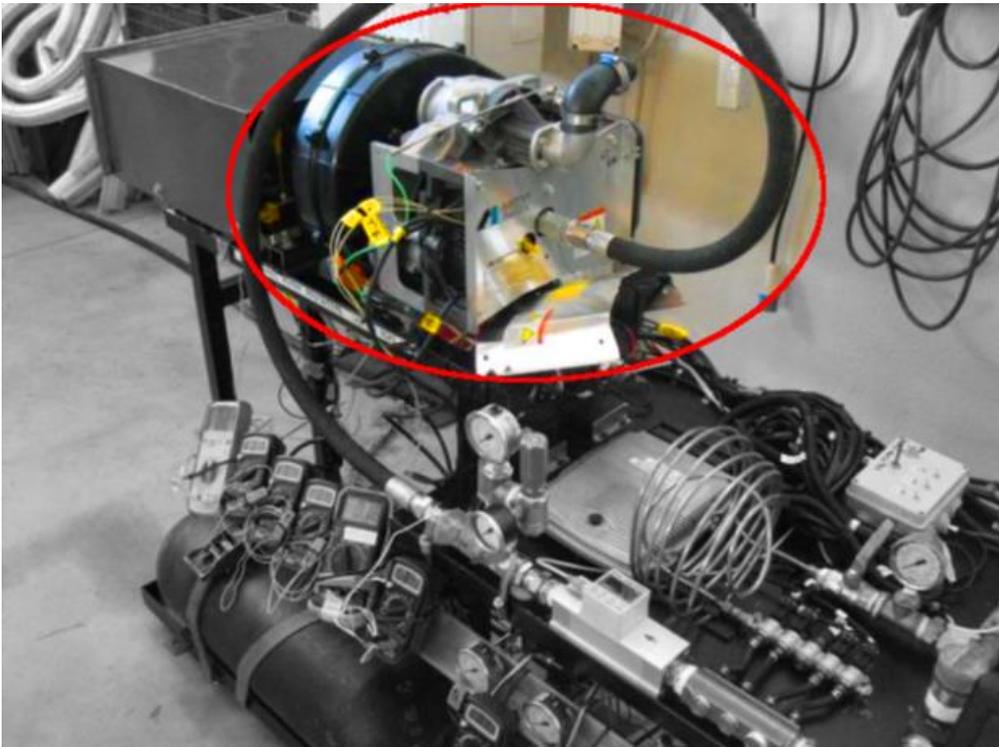
Nominal power	5.5 kW
Volume ratio	3.5
Displacement	73,000 mm ³ /rev
Rotational velocity	2600 rpm (MAX)
Flank gaps	20 – 100 μm

Scroll Test Bench

Experimental
campaign

Validation of
CFD process

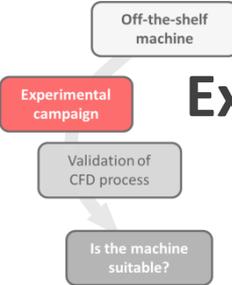
Is the machine
suitable?



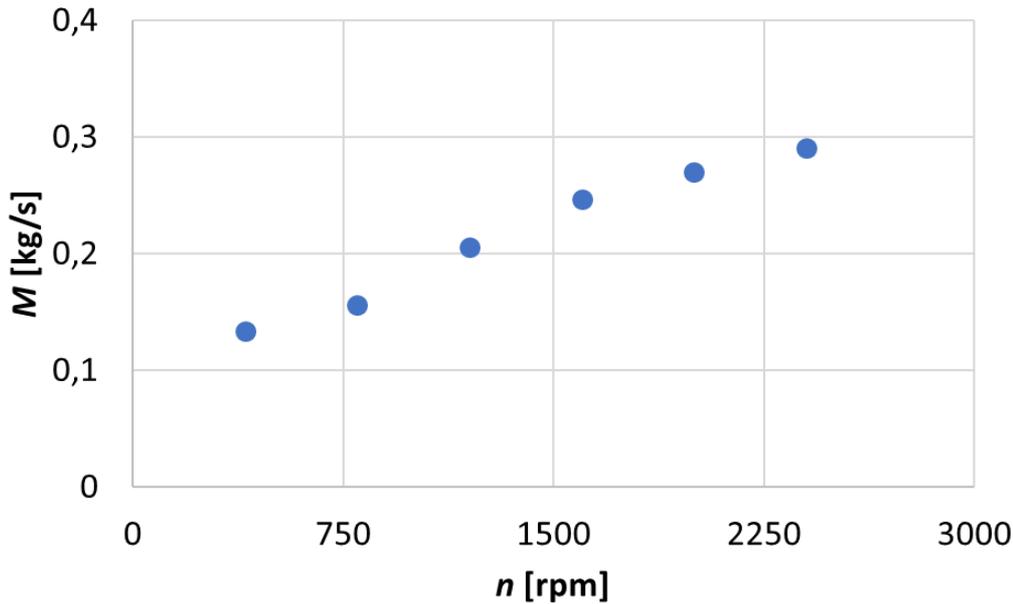
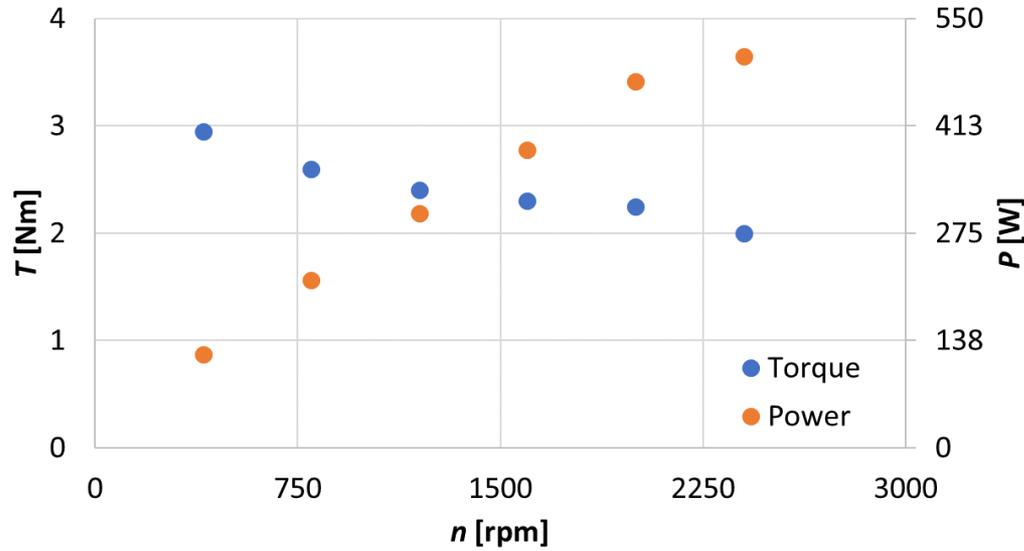
Pressure Transducers ($\pm 0.5 \% \text{ FS}$)
Temperature (A-class Pt100 probes)
Mass flow ($\pm 1.8 \% \text{ FS}$)
Load Cell ($\pm 0.05 \% \text{ FS}$)
Rotational speed
DAQ ($\pm 1 \text{ K}, \pm 1 \% \text{ R}$)

Operating conditions:

- Air
- p_{IN} : 7.5 bar
- T_{IN} : 292.15 K
- N: 400 rpm – 2400 rpm



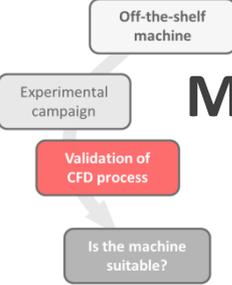
Experimental Results



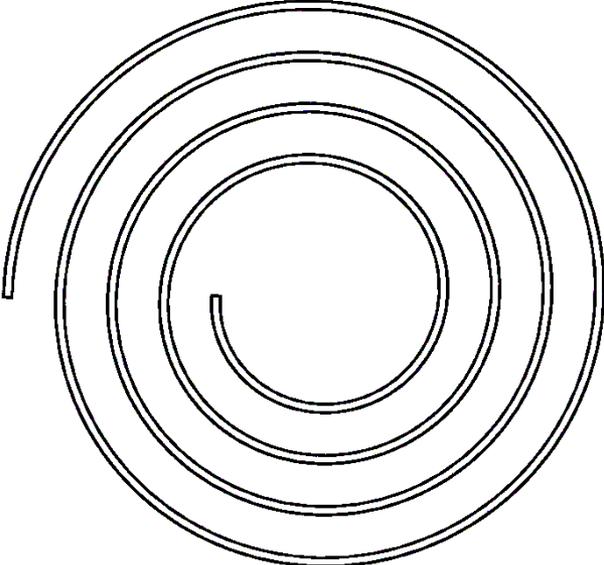
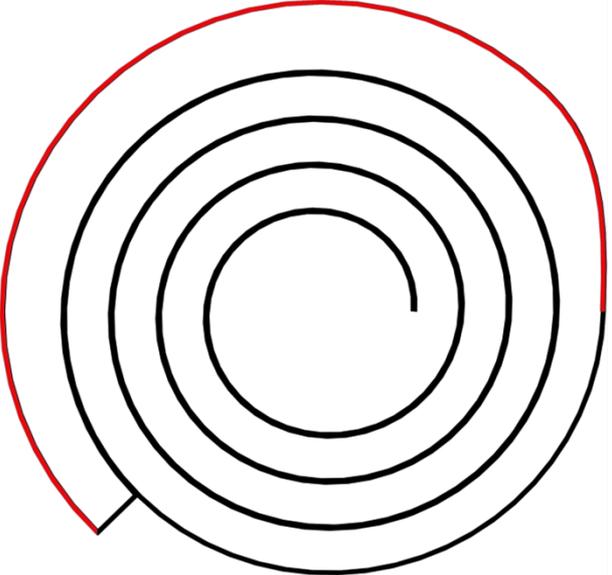
Trends were consistent with expectations



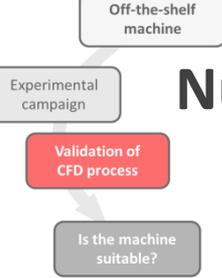
Model virtualization



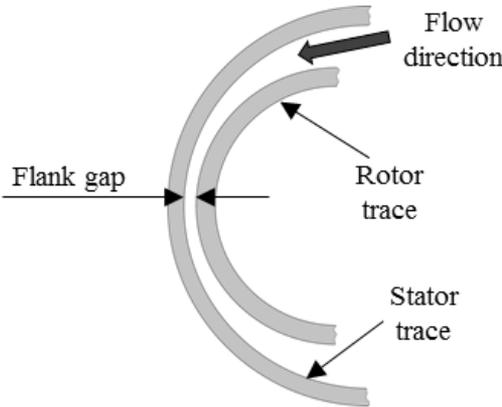
R.E. procedure



Numerical approach



Orbiting geometry with narrow **gaps**



↳ Overset mesh approach

↳ Great effort to generate a good quality mesh

- Polyhedral elements at the core
- Prismatic cell layers on moving walls

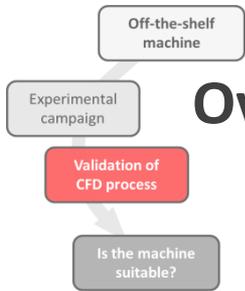


Number of mesh elements $> 21 \cdot 10^6$

Quality > 0.2



Overset grid



Two independent grids are used to discretize the computational domain

Moving grid has to:

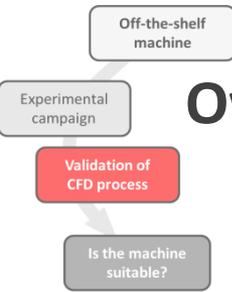
- Follow the domain geometry modification by means of a rigid body motion
- Exchange information with fixed grid by means of several local “interfaces” (donor and acceptor cells)

To establish the connectivity between the grids, a two-step Overset Assembly process takes place:

- 1- Hole-cutting, which determines which cells are active, inactive, or acceptor cells
- 2- Donor Search, which ensures that donor cells are found for each acceptor cell

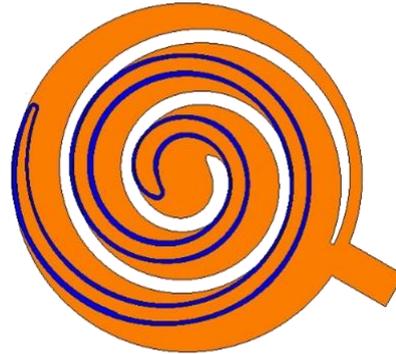


In a scroll machine, this process is not trivial!

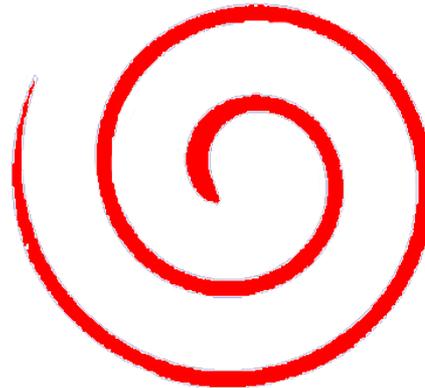


Overset strategy applied to scroll

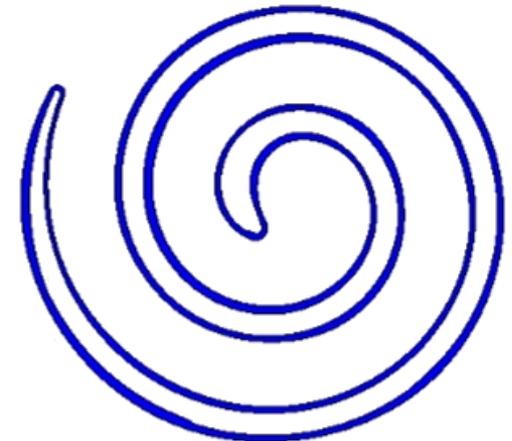
All points
(background and overlapping grid)



Active points
(called field point)

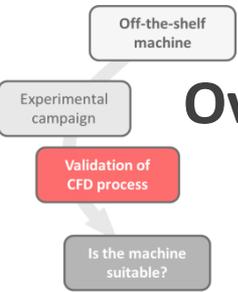


Hole points
(related to inactive cells)

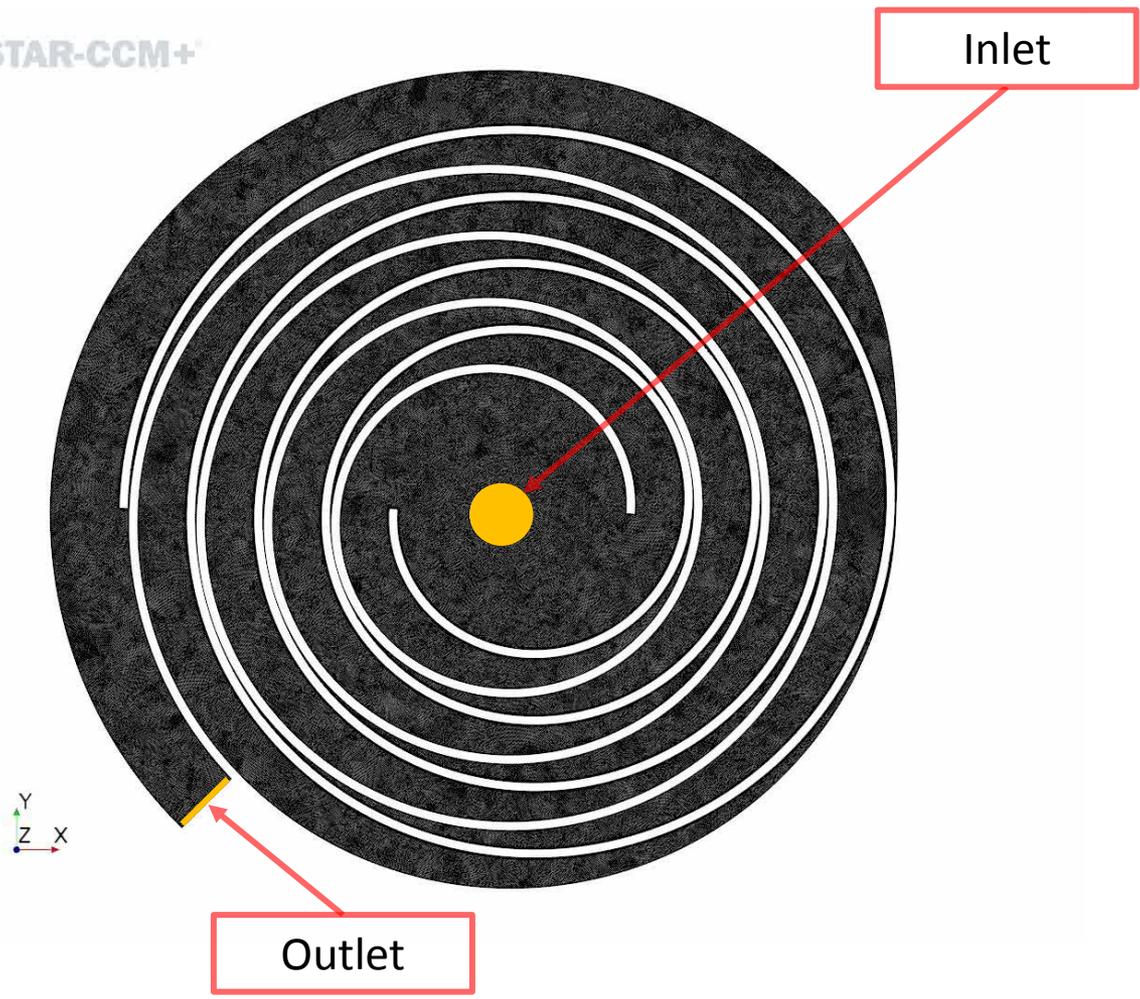


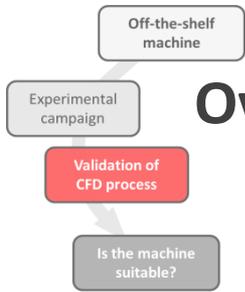
Receptor (acceptor) points
(data interpolation with the overset cells)





Overset grid – 3





Overset grid – 4



The element quality in the gaps is completely defined
(after the grid generation, each cells remains the same)



The grid morphology remains the same
(no element deformation is needed)



Matching between the Background and overset grid is critical
(5 elements with similar size at least)



Two numerical domains at least (background + overset)
(each moving object needs its overset grid)



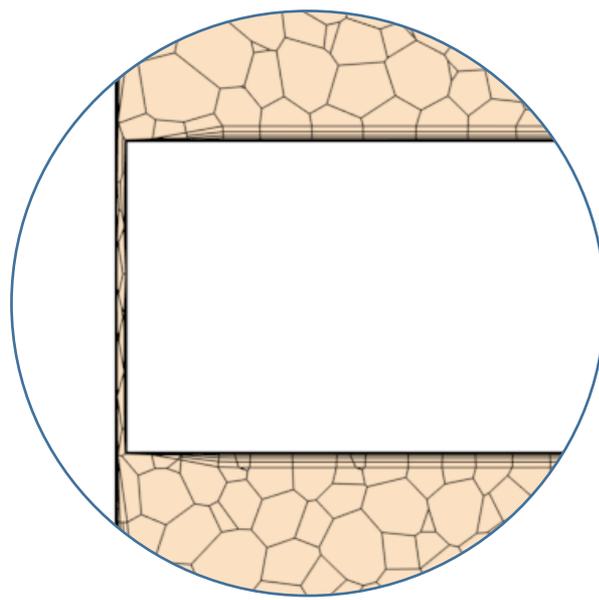
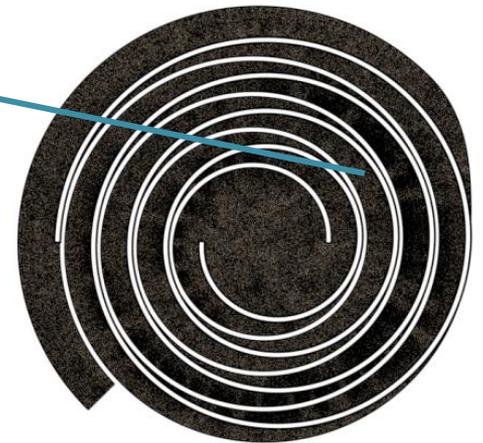
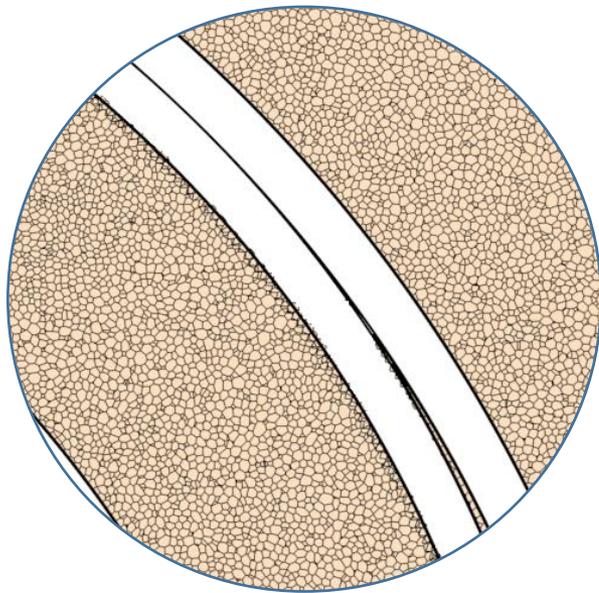
Off-the-shelf machine

Experimental campaign

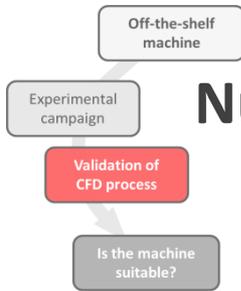
Validation of CFD process

Is the machine suitable?

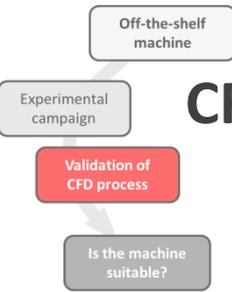
Numerical model



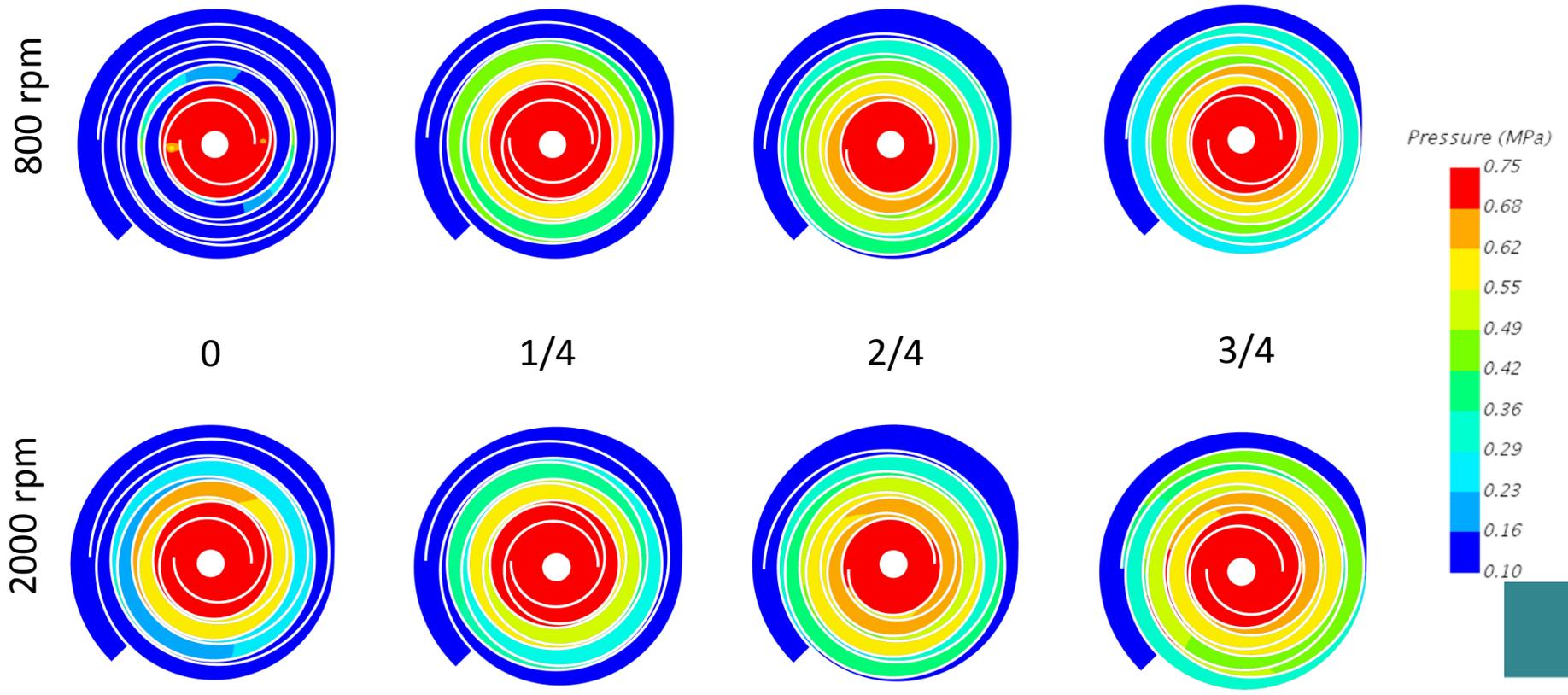
Numerical model - Air

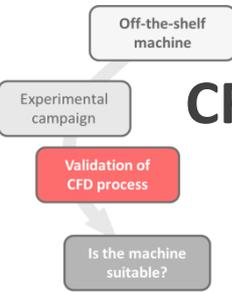


- Siemens STAR-CCM+ 11.02
- Flow: Compressible, 3D
- Gas: Air as a real gas
- Real gas model: Redlich-Kwong
- Turbulence model: 2nd order Realizable k- ϵ , two-layer y^+ wall treatment
- Temporal discretization: 1st order, $5 \cdot 10^{-6} s$ time-step
- Boundary conditions:
 - Inlet pressure: 7,5 *bar*
 - Inlet temperature: 292,15 *K*
 - Outlet pressure: 1,01 *bar*
 - Walls thermal specification: adiabatic.



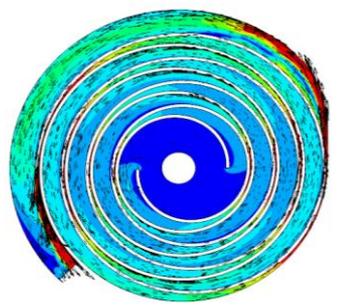
CFD: Air – Pressure



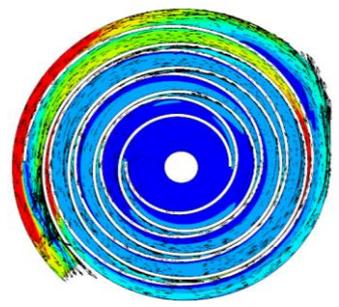


CFD: Air – Volume flow

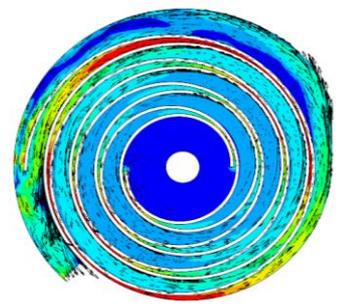
1600 rpm



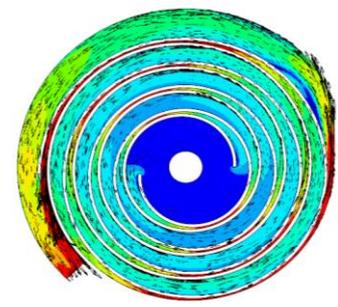
0



1/4

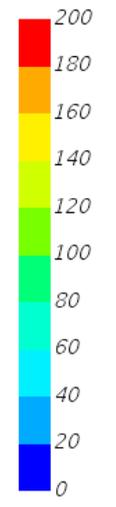


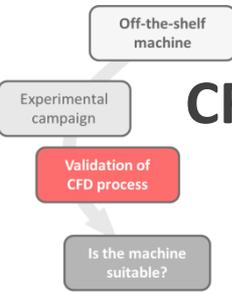
2/4



3/4

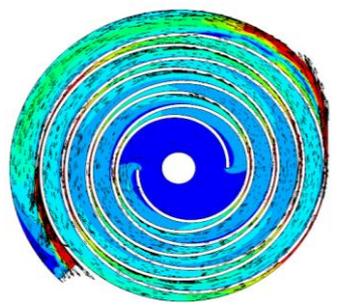
Velocity: Magnitude (m/s)



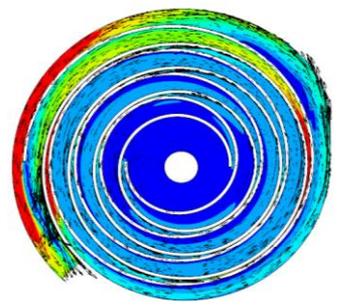


CFD: Air – Volume flow

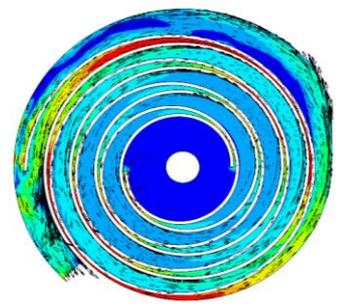
1600 rpm



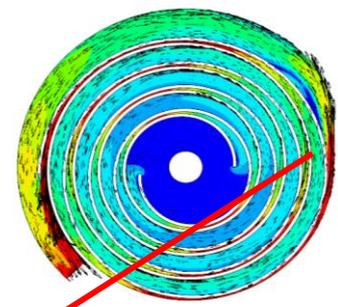
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1/4

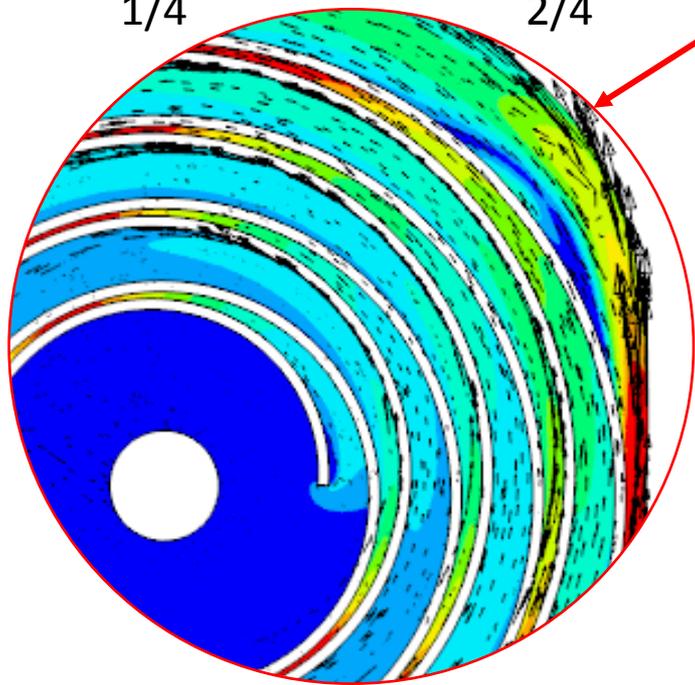
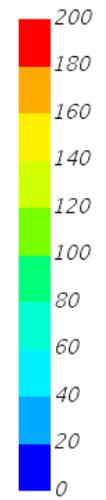


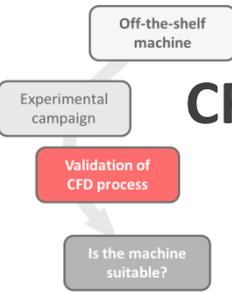
2/4



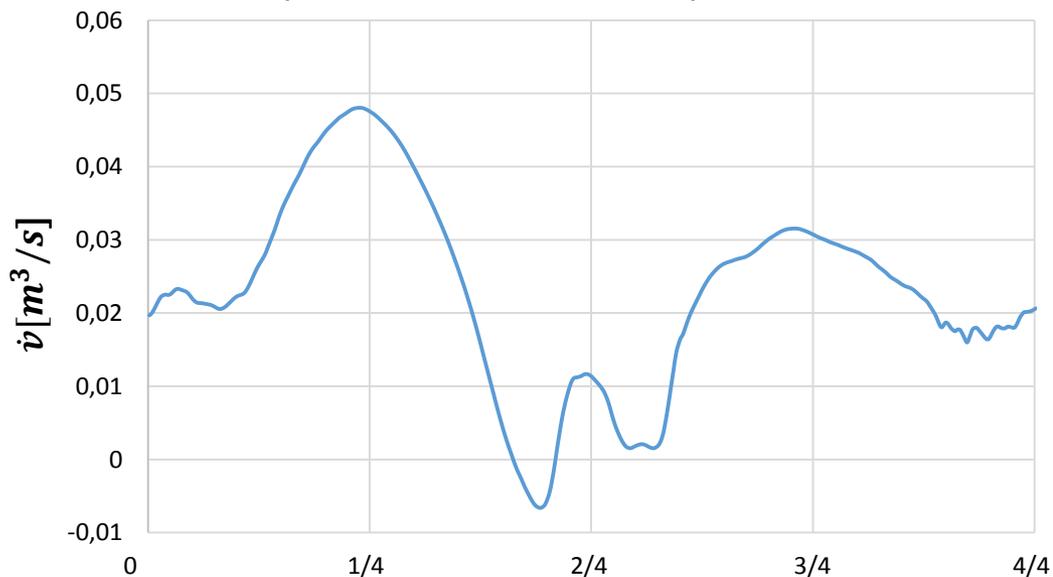
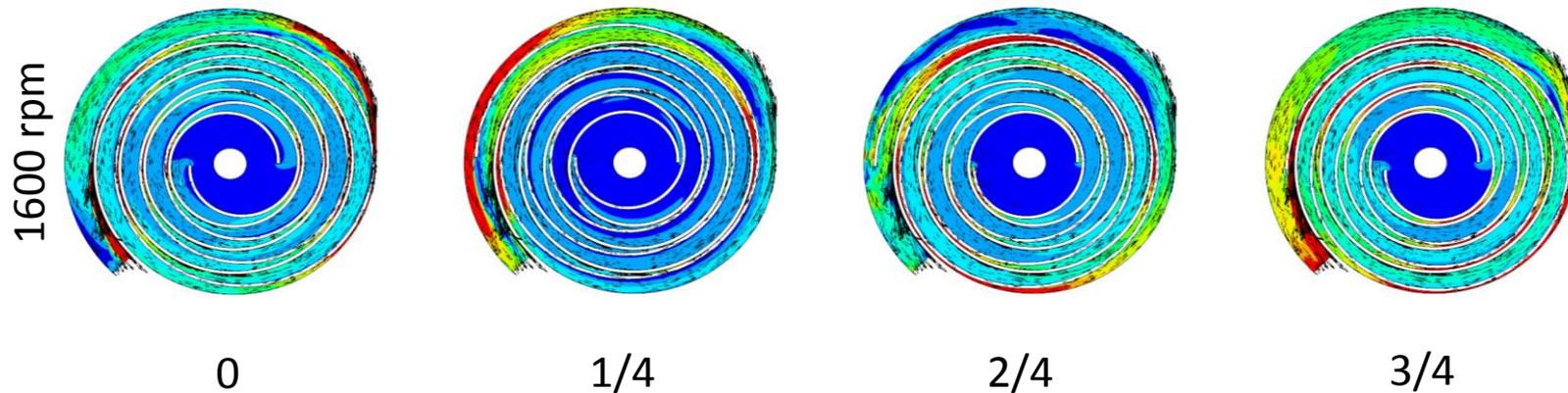
3/4

Velocity: Magnitude (m/s)





CFD: Air – Volume flow – 2



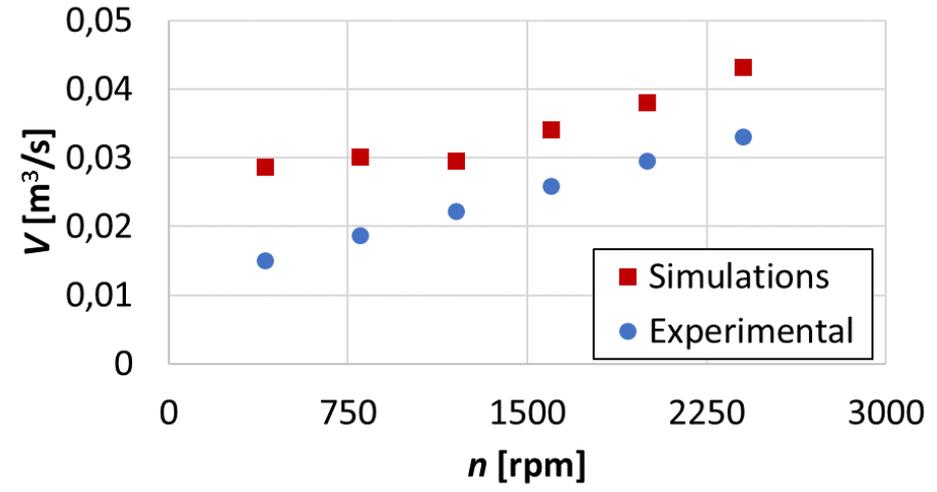
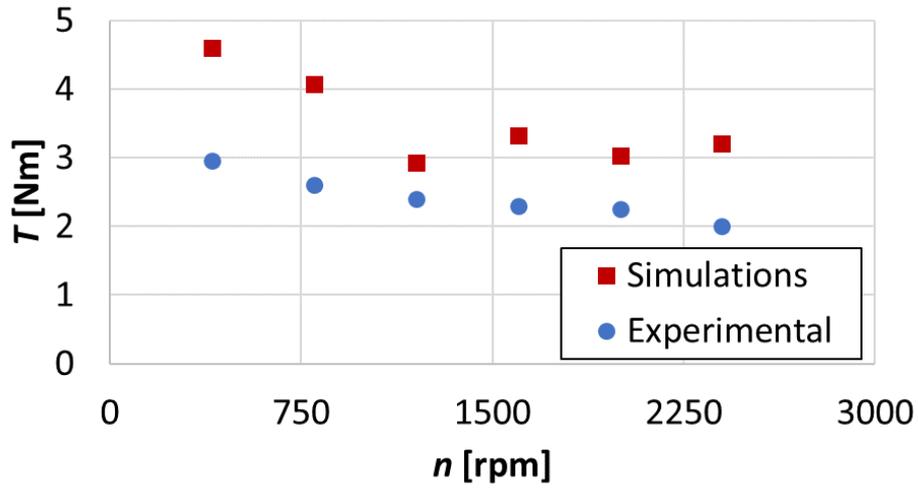
Off-the-shelf machine

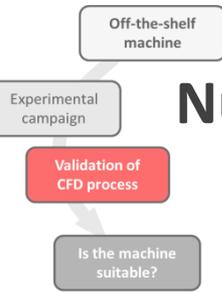
Experimental campaign

Validation of CFD process

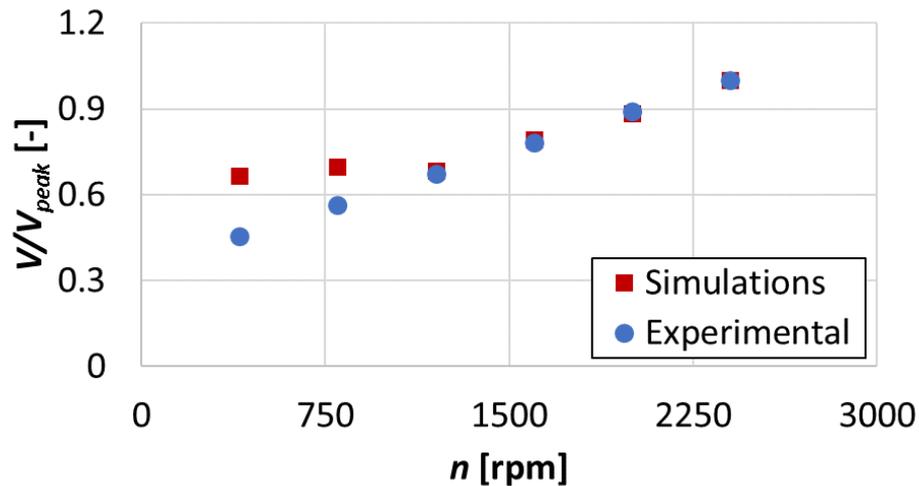
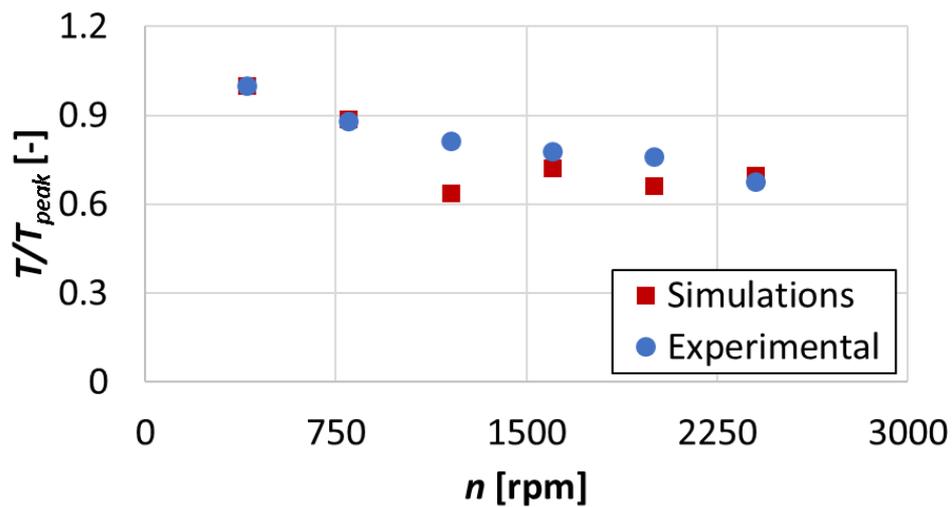
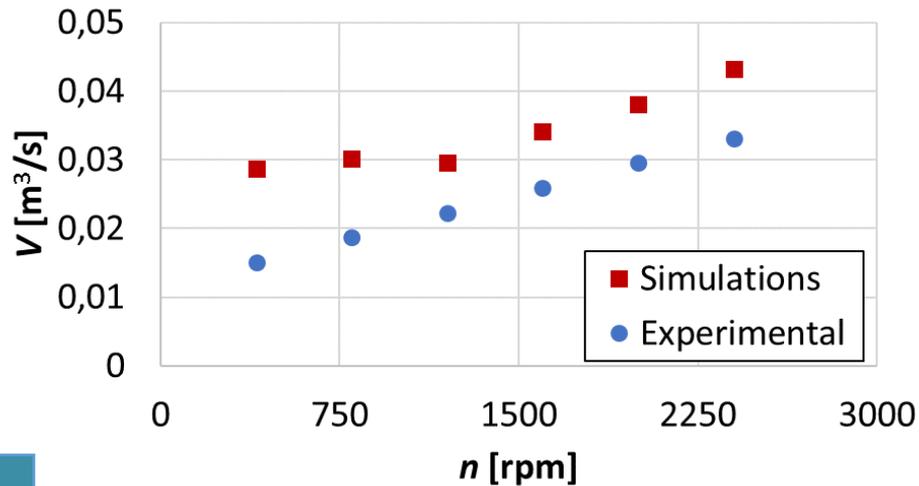
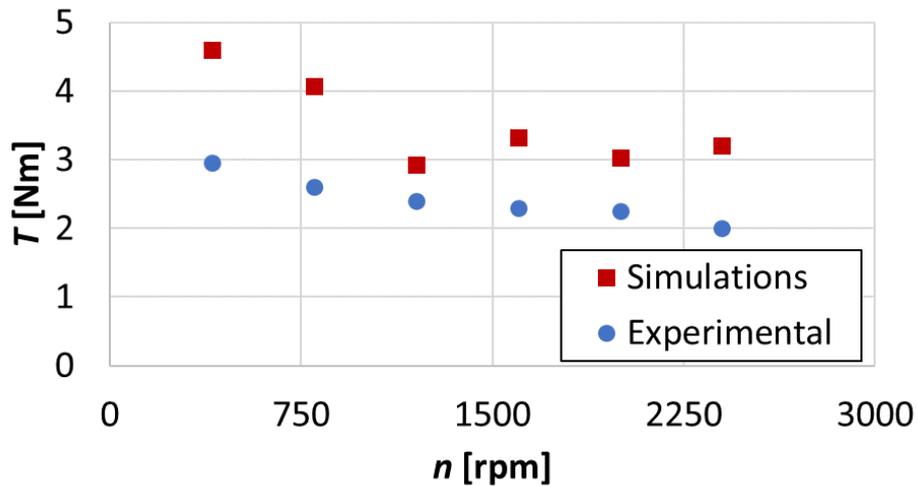
Is the machine suitable?

Numerical vs Experimental results





Numerical vs Experimental results



Off-the-shelf machine

Experimental campaign

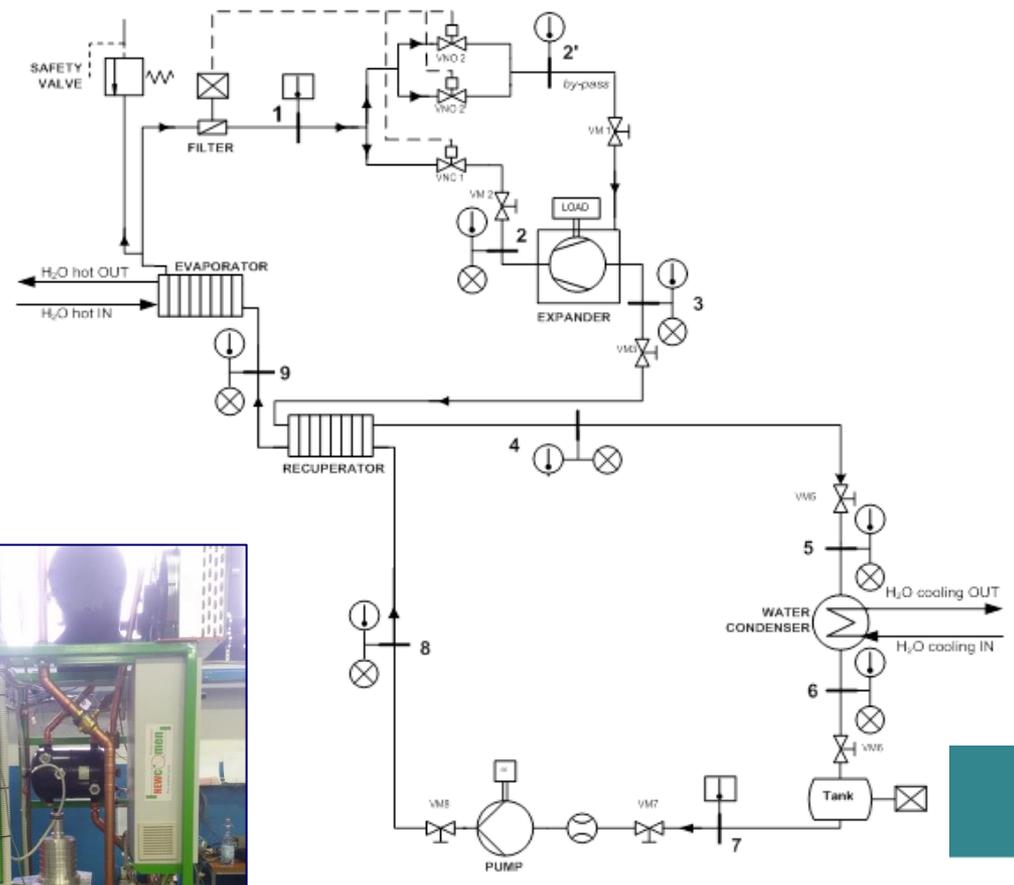
Validation of CFD process

Is the machine suitable?

Application to an actual ORC system



Actual expander:
Piston



Off-the-shelf machine

Experimental campaign

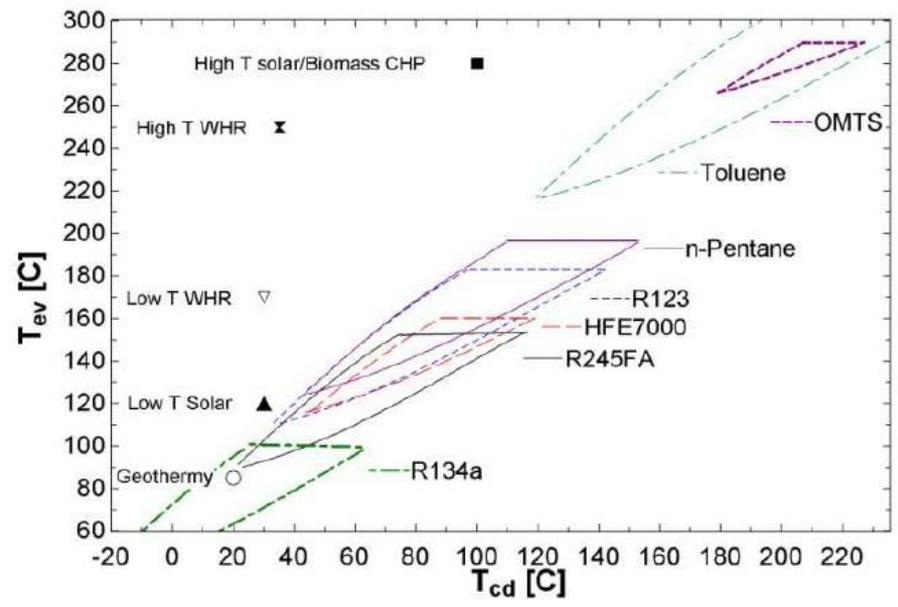
Validation of CFD process

Is the machine suitable?

Numerical model with R134a



Which machine is suitable for actual operating conditions?



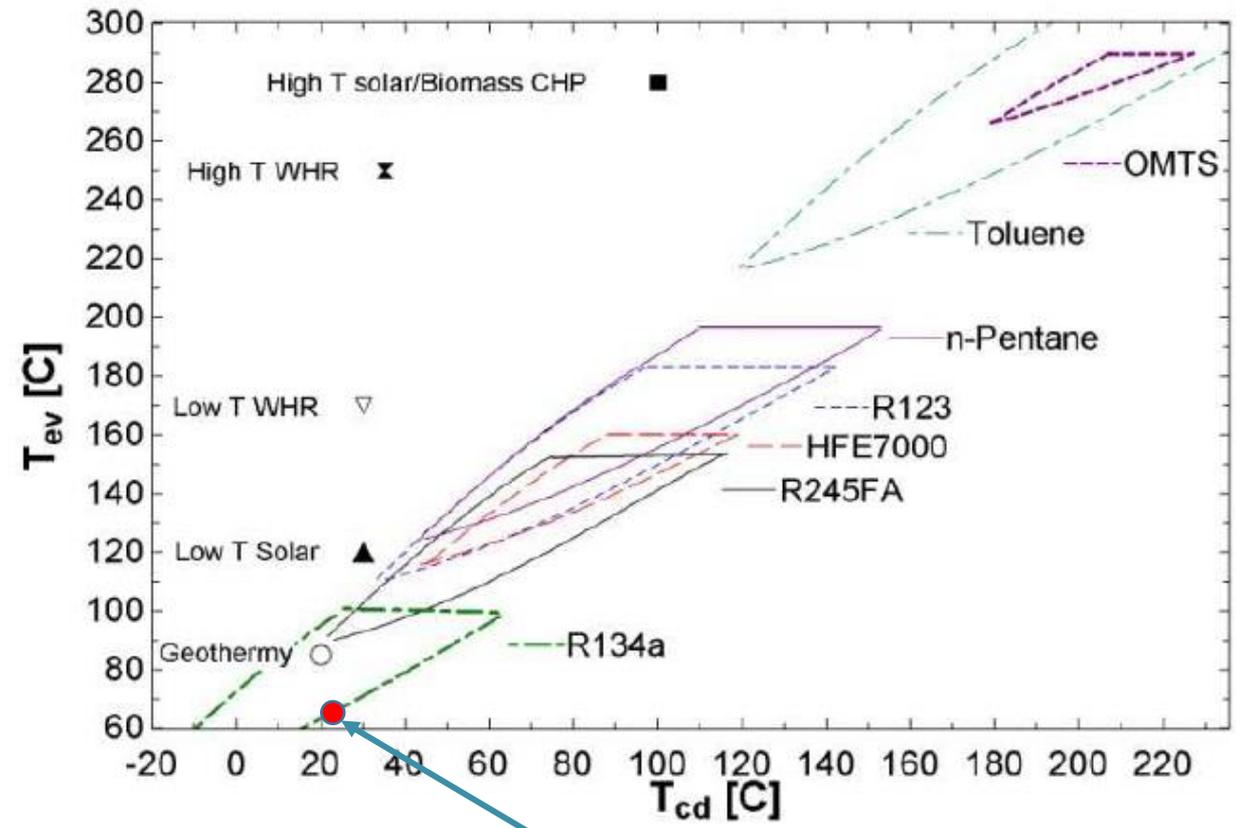
Off-the-shelf machine

Experimental campaign

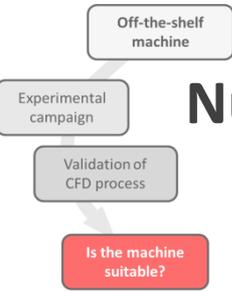
Validation of CFD process

Is the machine suitable?

Numerical model with R134a



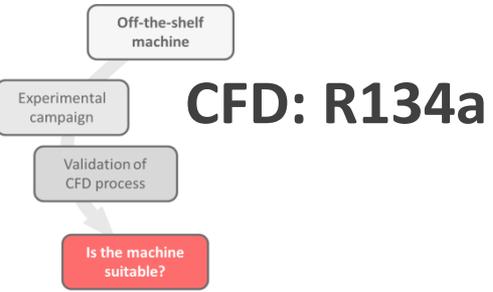
Our cycle



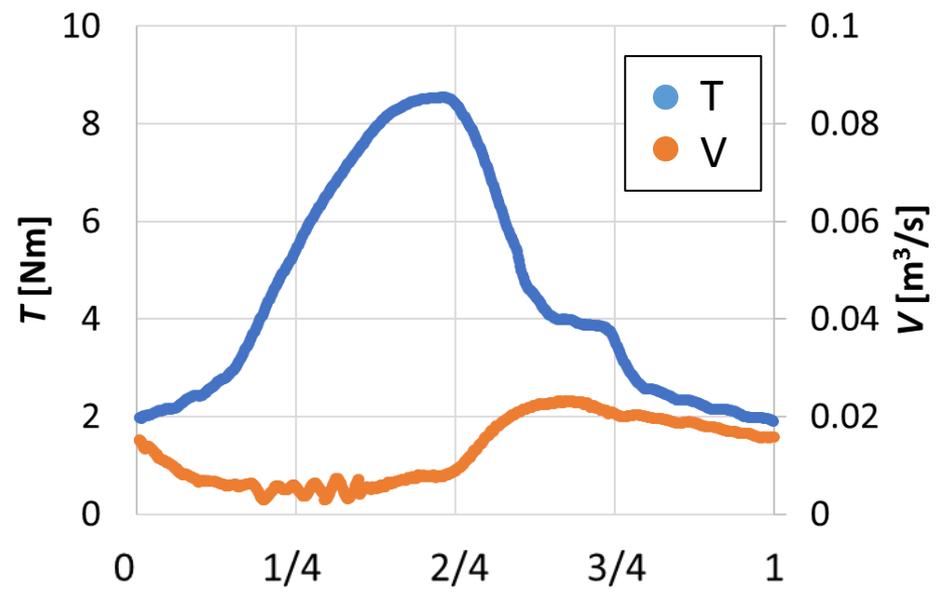
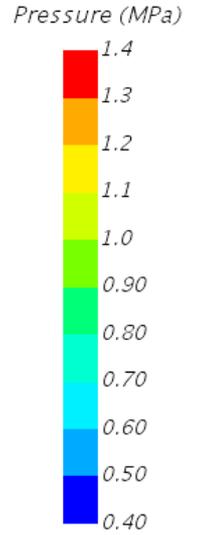
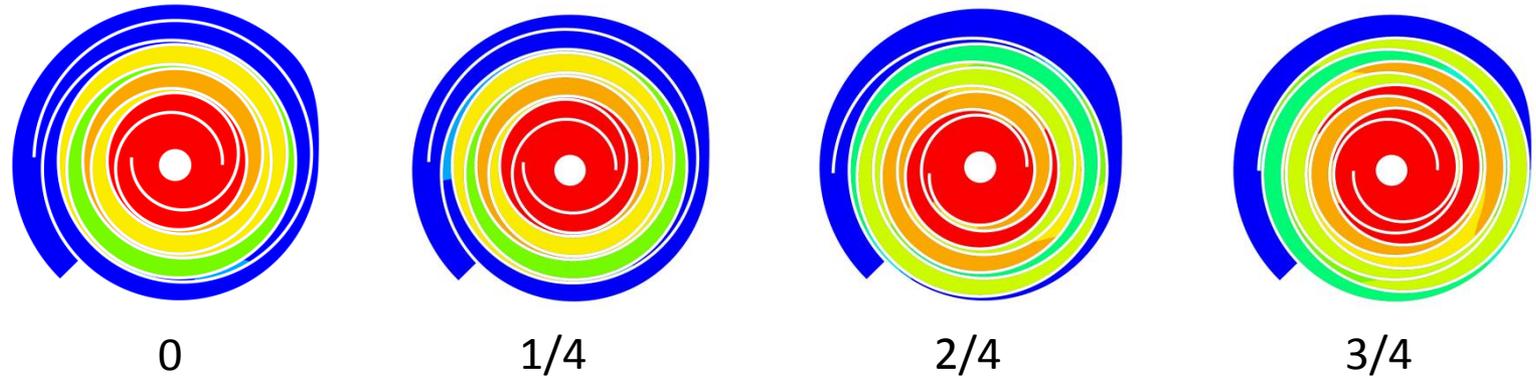
Numerical model – R134a

- Siemens Star-CCM+ 11.02
- Compressible, 3D, Finite Volume Solver
- Temporal discretization: 1st order, $1 \cdot 10^{-6}$ s time-step ←
- Gas: R134a ←
- Real gas model: Redlich-Kwong
- Turbulence model: 2nd order Realizable k- ϵ , two-layer y^+ wall treatment
- Boundary conditions:
 - Inlet pressure: 13,9 bar ←
 - Inlet temperature: 338 K ←
 - Outlet pressure: 4,00 bar ←
 - Walls thermal specification: adiabatic.

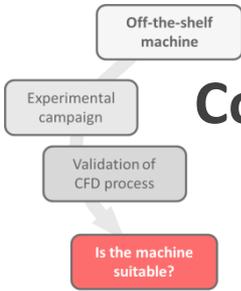




CFD: R134a



Conclusions

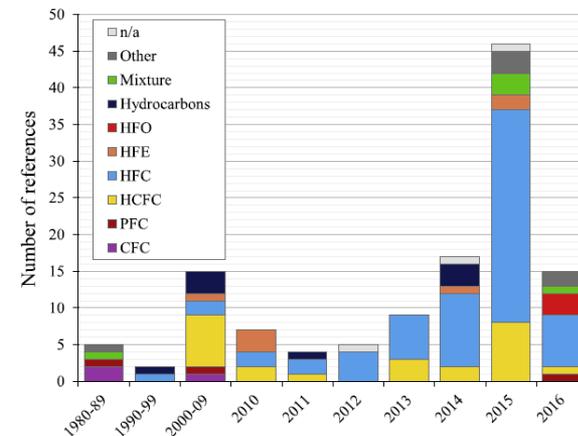


- CFD analysis was able to capture flow and torque trends, while calculated values showed a certain deviation when compared to the measured ones
 - ↳ Great influence of gaps and their modeling
 - Better results can be obtained by reducing gaps width in the model
 - ↳ Greater computational effort
- CFD analysis showed fluctuations in the output torque and volume flow for the real gas expansion case
 - ↳ Vibrations and noise are critical for household equipment

Future development

- Numerical simulations of the pump
- Expander and pump performance for different working fluids (current issue)

↳ Maximize cycle efficiency



- Study of different types of expanders as cycle components

↳ Single-screw expander



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DE Department of
Engineering
Ferrara

Thank you

4th International seminar on
ORC Power Systems

