IV International Seminar on ORC Power Systems





POLITECNICO MILANO 1863

Selection Maps For ORC And CO₂ Systems For Low-Medium Temperature Heat Sources

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>> INTRODUCTION (1) A father of two technologies

Professor Angelino was one of the father of both ORC and sCO₂ technologies

In the second half of last century the pioneering studies of Profesor Angelino set the standard for:

- fluid selection criteria and effect on turbomachinery design for ORC field
- Best cycle configurations and optimal design for sCO₂ power systems

The results obtained in those studies are the reference benchmark still today



>> INTRODUCTION (2) from a clear division...

<u>ORC</u>

- Low temperature heat sources like geothermal energy, solar energy with low concentrating ratio and OTEC systems
- Small available heat like in civil and domestic cogeneration, small WHR application and biomass



High temperature and Large available heat applications like nuclear, solar towers and recently fossil fuels

Until recent years ORC and sCO_2 cycles have been studied for two **completely different** application fields as alternative for steam power plants:

>> INTRODUCTION (3) ...to the need of clarity

<u>ORC</u>

- Low temperature heat sources like geothermal energy, solar energy with low concentrating ratio and OTEC systems
- Small available heat like in civil and domestic cogeneration, small WHR application and biomass



High temperature and Large available heat applications like nuclear, solar towers and recently fossil fuels

Nowadays the scenario is **strongly changed**:

- Many organic fluids for ORC applications are going trough a phase out process because of their environmental impact (high GWP) or safety reasons (flammability and toxicity)
- sCO₂ is experiencing large investments mainly driven by CSP field that will bring soon this technology to a mature technological level

>> INTRODUCTION A new GREY ZONE

As result this division will become more and more blurred in future years with ORC and sCO_2 power plants **competing** in a large range of applications

VS

• Large biomass plant

ORC

- Large and high temperature WHR (glass, steel, cement industries)
- Medium size CSP plant based mainly based on linear concentrators

As result a NEW GREY ZONE is coming

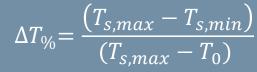
>> WORK BASIS Aim of the study and General approach

Our goal:

- Understanding which is the most suitable solution among ORC and sCO₂ for different energy sources and applications
- providing decision maps for the correct choice of the best plant from a thermodynamic point of view

Our approach:

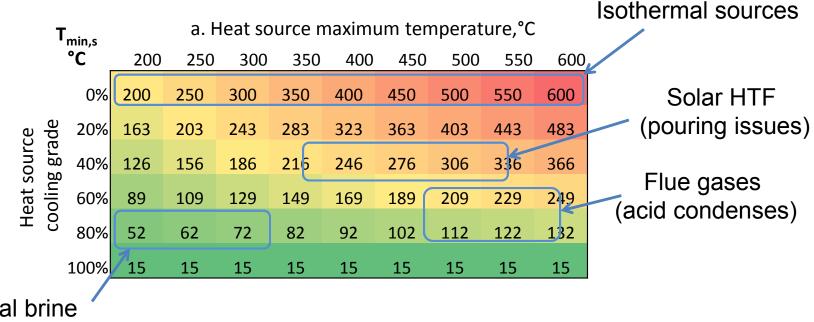
- We defined the optimal ORC and optimal sCO₂ cycle for a large range of energy sources differing in:
 - ➤ maximum temperature (250°C 600°C)
 - ➤ cooling grade (0% 100%)



- Available power is fixed and equal to 30 MW with reference to medium- large size applications
- Two cases are investigated: air and water cooled plants with possibility to condensate CO₂

>> MAP RANGE Heat source characterization

This allows to represent both nearly isothermal heat sources and finite heat capacity heat sources with technical limits in the minimum temperature



Geothermal brine (silica deposition)

>> DESIGN CRITERIA Organic Rankine Cycles

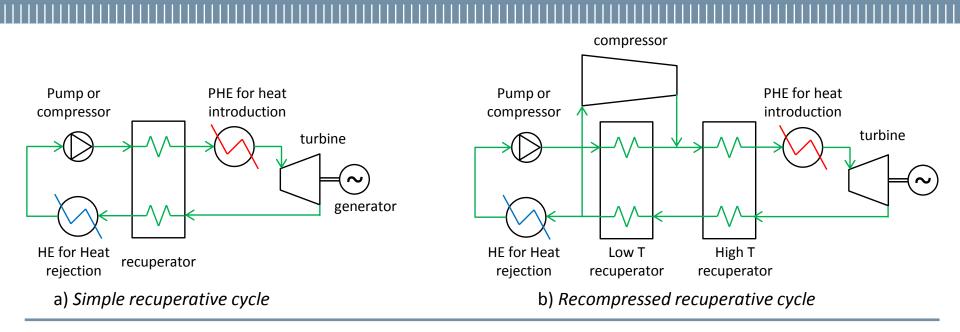
4 Cycle configurations:

- saturated and superheated subcritical with or without recuperator
- 47 working fluids:

15 alkanes, 8 other HC, 16 halogenated, 8 siloxanes

- Large range of **critical temperatures** and **molecular complexity**
- Maximum temperature is set by thermal stability limit or lack of experimental data.
- Minimum pressure is set to 1 bar in order to avoid air leakage
- Optimization variables T_{eva}, T_{cond}, T_{inTurbine}

>> DESIGN CRITERIA sCO2 cycles



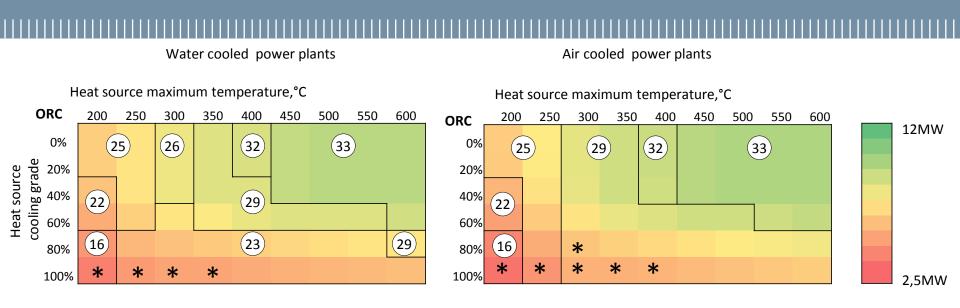
- Recompressed cycle allows to limit the temperature differences in the recuperative process
- Water cooled plant allows for CO₂ condensation leading to an increase of power output
- Optimization variables p_{max (UB=300bar)}, p_{min}, split ratio

>> DESIGN CRITERIA Common Assumptions

	C	CO ₂ ORC		2
Heat sink temperature	15°C water cooled	25°C air cooled	15°C water cooled	25°C air cooled
Minimum working fluid temperature	25°C	40°C	25°C	40°C
$\Delta T_{ap,PHE} \Delta T_{pp,PHE} \Delta T_{pprec}$	10)°C	5°C	
ΔT _{subcooling}		-	5°C	
Δp(or, whether relative, Δp/p _{in}) PHE	2	%	50kPa (ECO), ΔT=1°C (EVA), 2% (SH)	
Δp (or, whether relative, Δp/p _{in}) REC	2% (hot side), 2% (cold side)		2% (hot side), 50 kPa (cold side)	
Δp(or, whether relative, Δp/p _{in}) HR	2	%	2% (desuperheating), ΔT=0.5°C (condensation)	
Compressor/pump hydraulic efficiency	0.	85	0.75	
Generator electrical efficiency	0.97			
Mechanical efficiency	0.97			
Pump electrical motor efficiency	0.	97	0.97	
Auxiliaries consumption loss	2%			

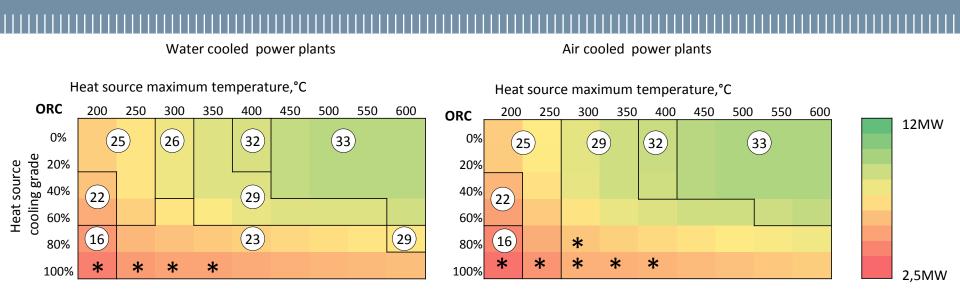
Turbine efficiency is computed as function of SP and Vr

>> RESULTS Organic Rankine Cycles



- Power production is higher for high temperature heat sources with a low cooling grade,
- Power production is limited for heat sources temperatures higher than 450°C because of the fluid thermal stability limit
- Power production is lower for air cooled plants because of the higher condensation temperature

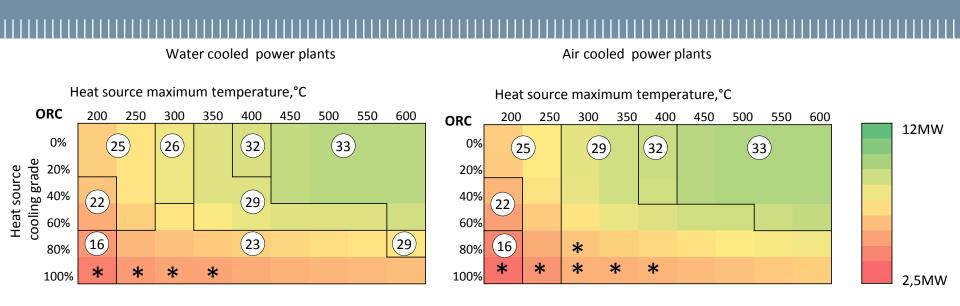
>> RESULTS Organic Rankine Cycles



 Best fluid critical temperature increases with the heat source temperature and for nearly isothermal heat sources

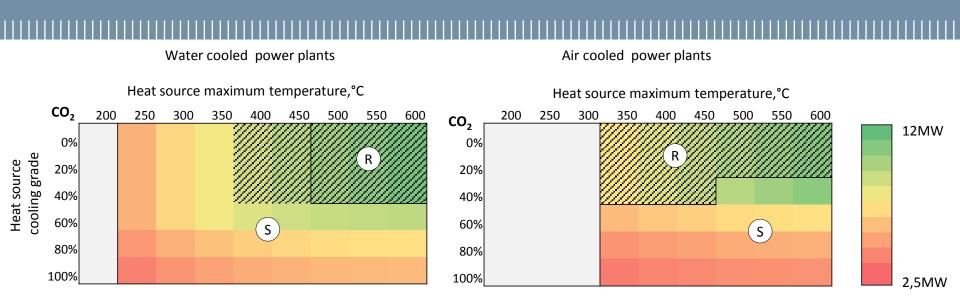
16 – R236ea	139°C	26 – pentane	197°C
22 – neo pentane	161°C	29 – cyclo pentane	239°C
23 – cis butene	163°C	32 – cyclo hexane	280°C
25 – iso pentane	187°C	33 – benzene	289°C

>> RESULTS Organic Rankine Cycles



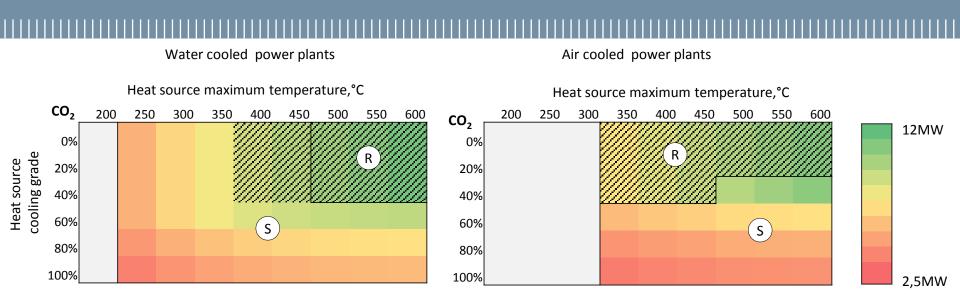
- Superheated recuperative cycle is always convenient however..
 - saturated cycles can be competitive for low temperature sources with small cooling grade
 - Recuperator is not convenient for low-medium temperature heat sources with high cooling grades (marked with*)

>> RESULTS sCO₂ cycles



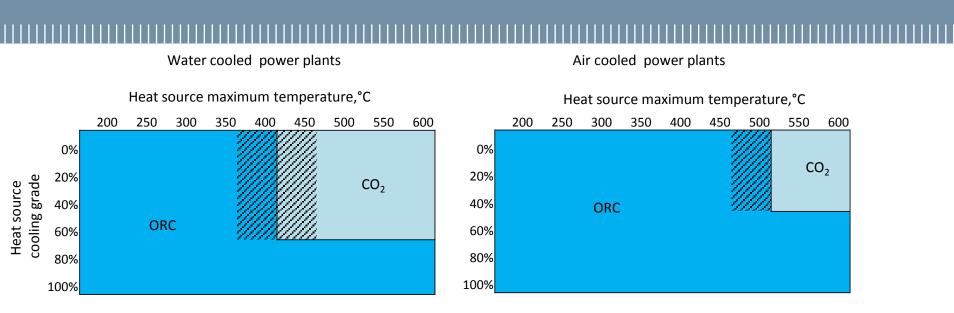
- Power production always increases reaching thanks to CO₂ stability at high temperatures
- Power production strongly penalized for air cooled plants because condensation is not possible. Positive net power is obtained for heat sources temperatures higher than 300°C

>> RESULTS sCO₂ cycles



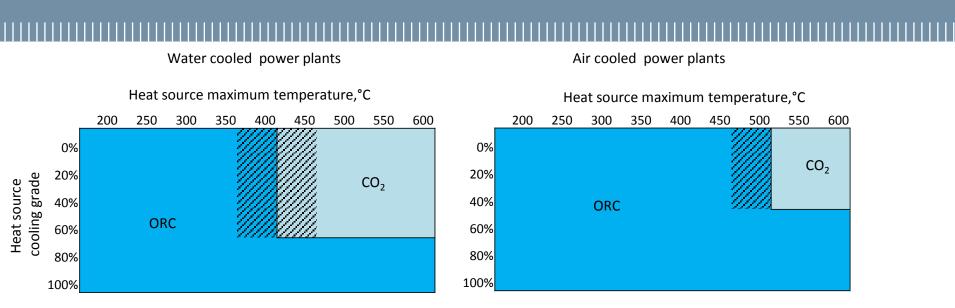
- Recompressed cycle (R) performs better than simple recuperative cycle (S) for high temperatures and nearly isothermal heat sources
- The advantages in adopting a more complex configuration are limited and the two cycles have similar power outputs (2% difference) in the shaded area

>> RESULTS ORC vs sCO2



- For water condensed cycles ORC are recommended for :
 - heat sources temperatures below 350°C
 - for hotter heat sources having high cooling grades thanks to their ability to recover heat at low temperatures

>> RESULTS ORC vs sCO₂



- sCO₂ cycles are more efficient for high temperatures thanks to the increase of turbine power output respect to the compressor consumption
- Air cooling strongly penalizes sCO₂ that becomes convenient only for a very limited number of applications

>> CONCLUSIONS based on preliminary results

- sCO₂ cycles are certainly a reliable option for high temperature large power plants while they must compete with ORC in other applications
- Performances attainable by sCO₂ also at lower temperatures and for medium size application can be attractive especially in presence of particular constraints related to safety.
- Excluding flammable and toxic fluids CO₂ prevails also at low temperature (350°C)and high cooling grades
- Analysis should be extended to other sCO₂ plant configurations
- Analysis should be extended to economic analysis in order to catch the reduction of power plant capital cost allowable with compact CO₂ cycles

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THANKS FOR THE ATTENTION

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